

Problem Set # 6

1. Since $V_{BS} = -1$ first we need to find the new threshold voltage (V_{Tn})

$$V_{Tn} = V_{T0n} + \gamma_n (\sqrt{-2\phi_p - V_{BS}} - \sqrt{-2\phi_p})$$

$$= 1\text{V} + 0.6 (\sqrt{0.84 + 1} - \sqrt{0.84}) = 1.26\text{V}$$

Since $V_{GS} = 3\text{V}$ is bigger than $V_{Tn} = 1.26\text{V}$ and

$V_{DS} = 5\text{V}$ is bigger than $V_{GS} - V_{Tn} = 1.74\text{V}$, the nMOS is in saturation, as expected.

Note that channel length modulation is ignored to make the calculations simpler

$$I_D = \frac{W}{2L} \mu_n C_{ox} (V_{GS} - V_{Tn})^2 = \frac{22}{2 \times 1.8} 50 \frac{\mu\text{A}}{\text{V}^2} (3\text{V} - 1.26\text{V})^2 = \underline{925 \mu\text{A}}$$

note that $L = L_{\text{gate}} - 2L_D = 2.0 \mu\text{m} - 0.2 \mu\text{m} = 1.8 \mu\text{m}$

a)

$$g_m = \sqrt{2 \frac{W}{L} \mu_n C_{ox} I_D} = \sqrt{2 \frac{22}{1.8} 50 \times 10^{-6} \times 925 \times 10^{-6}} = \underline{1063 \mu\text{S}}$$

$$g_{mb} = \frac{\gamma_n g_m}{2\sqrt{-2\phi_p - V_{BS}}} = \frac{0.6 \times 1063 \times 10^{-6}}{2\sqrt{0.84 + 1}} = \underline{235 \mu\text{S}}$$

$$g_o = \frac{1}{r_o} = \lambda_n I_D = \frac{0.1}{1.8} \times 925 \times 10^{-6} = \underline{51 \mu\text{S}} \Rightarrow r_o = \underline{19.5 \text{ k}\Omega}$$

b)

$$C_{gs} = \frac{2}{3} W L C_{ox} + W C_{ov} \approx \frac{2}{3} W L C_{ox} + W L_D C_{ox} = \left(\frac{2}{3} L + L_D\right) W C_{ox}$$

$$= \left(\frac{2}{3} 1.8 \mu\text{m} + 0.1 \mu\text{m}\right) 22 \mu\text{m} \times 1.42 \text{ FF}/\mu\text{m}^2 = \underline{40.6 \text{ FF}}$$

$$C_{gd} = W C_{ov} \approx W L_D C_{ox} = 22 \mu\text{m} \times 0.1 \mu\text{m} \times 1.42 \text{ FF}/\mu\text{m}^2 = \underline{3.1 \text{ FF}}$$

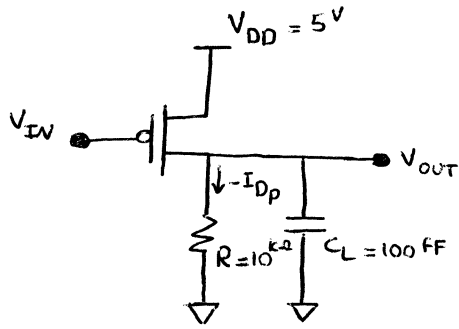
$$C_{sb} = W L_{\text{diff}} \sqrt{\frac{q \epsilon_s N_A}{2(\phi_B - V_{BS})}} = 22 \mu\text{m} \times 6 \mu\text{m} \sqrt{\frac{1.6 \times 10^{-19} \times 11.7 \times 8.85 \times 10^{-14} \times 10^{17}}{2(0.97 + 1)}}$$

$$= \underline{85.6 \text{ FF}}$$

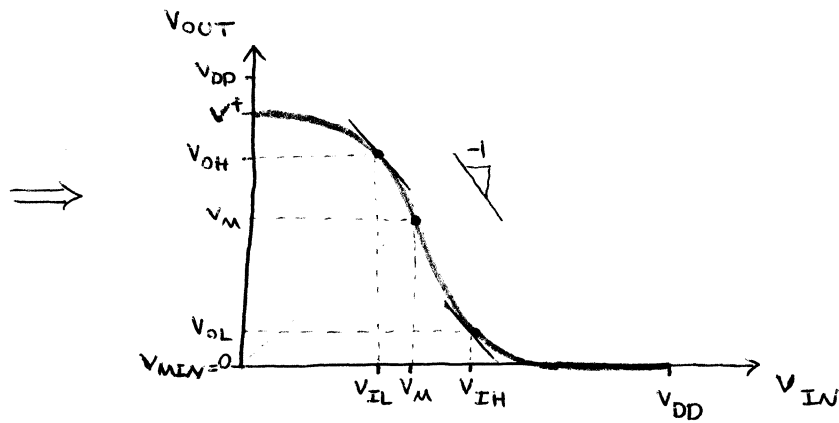
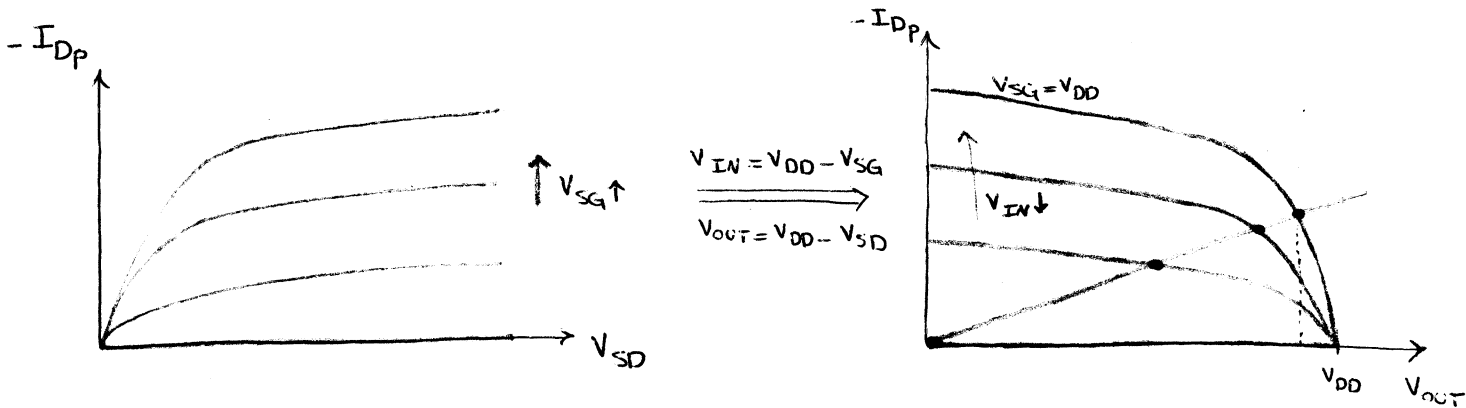
$$C_{db} = W L_{\text{diff}} \sqrt{\frac{q \epsilon_s N_A}{2(\phi_B - V_{BD})}} = 22 \mu\text{m} \times 6 \mu\text{m} \sqrt{\frac{1.6 \times 10^{-19} \times 11.7 \times 8.85 \times 10^{-14} \times 10^{17}}{2(0.97 + 6)}}$$

$$= \underline{45.5 \text{ FF}}$$

2.

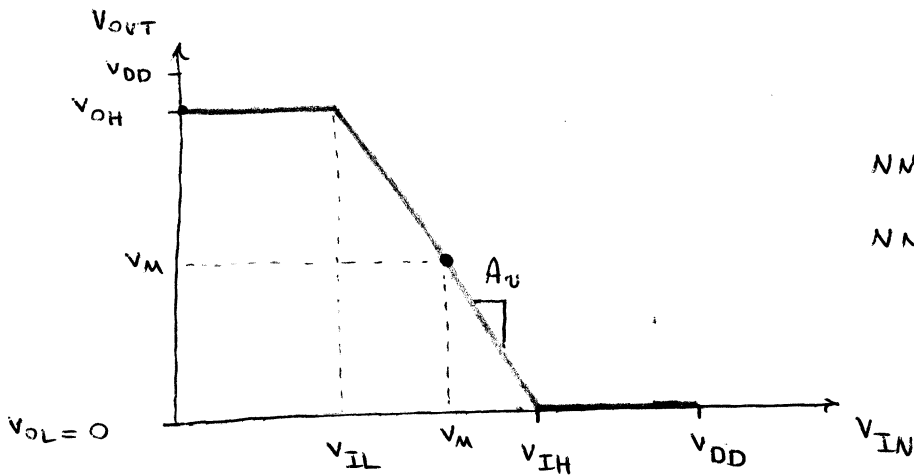


(a) The voltage transfer characteristic can be calculated from drain characteristics of the pMOS :



notice $V^+ < V_{DD}$ and $V_{MIN} = 0V$

b) In the simplified model the transfer characteristics is approximated by a piecewise linear function:



$$NM_H = V_{OH} - V_{IH}$$

$$NM_L = V_{IL} - V_{OL} = V_{IL}$$

at $V_{IN} = V_M$, where $V_{OUT} = V_M$, the pMOS is in saturation, there:

$$-I_{Dp} = \frac{W}{2L} \mu_p C_{ox} (V_{SG} + V_{Tp})^2 = I_R = \frac{V_{OUT}}{R}$$

$$\Rightarrow \frac{W}{2L} \mu_p C_{ox} (V_{DD} - V_M + V_{Tp})^2 = \frac{V_M}{R}$$

$$\Rightarrow \frac{20}{2 \times 1} 25 \times 10^{-6} (5 - V_M - 1)^2 = \frac{V_M}{10^4} \Rightarrow V_M^2 - 8.4 V_M + 16 = 0$$

$$\Rightarrow \underline{V_M = 2.9 \text{ V}}$$

$$\text{Also } -I_{Dp} = I_R = \frac{V_M}{R} = \frac{2.9 \text{ V}}{10 \text{ k}\Omega} = 290 \mu\text{A}$$

$$\begin{aligned} \text{therefore } g_m &= \sqrt{2 \frac{W}{L} \mu_p C_{ox} (-I_D)} = \sqrt{2 \frac{20}{1} 25 \times 10^{-6} \times 290 \times 10^{-6}} \\ &= 539 \mu\text{S} \end{aligned}$$

$$\text{so } A_v = -g_m (r_o \parallel R) \approx -g_m R = \underline{-5.39}$$

By knowing V_M and A_v we can calculate V_{IH} :

$$V_{IH} = V_M - \frac{V_M}{A_v} = 2.9^V + \frac{2.9^V}{5.39} = \underline{3.4^V}$$

To figure out V_{OH} we need to write down the equation for drain current at $V_{IN} = 0$ ($V_{OUT} = V_{OH}$). since the pMOS is in triode regime at this point:

$$\frac{W}{L} \mu_p C_{ox} \left(V_{SG} + V_{TP} - \frac{V_{SD}}{2} \right) V_{SD} = \frac{V_{OUT}}{R}$$

$$\Rightarrow \frac{W}{L} \mu_p C_{ox} \left(V_{DD} + V_{TP} - \frac{V_{DD} - V_{OH}}{2} \right) (V_{DD} - V_{OH}) = \frac{V_{OH}}{R}$$

$$\Rightarrow \frac{W}{2L} \mu_p C_{ox} (V_{DD} + 2V_{TP} + V_{OH}) (V_{DD} - V_{OH}) = \frac{V_{OH}}{R}$$

$$\Rightarrow \frac{20}{2 \times 1} 25 \times 10^{-6} (5 - 2 + V_{OH}) (5 - V_{OH}) = \frac{V_{OH}}{10^4}$$

$$\Rightarrow V_{OH}^2 - 1.6 V_{OH} - 15 = 0 \Rightarrow \underline{V_{OH} = 4.8^V}$$

therefore

$$V_{IL} = \frac{1 - A_v}{-A_v} V_M - \frac{V_{OH}}{-A_v} = \frac{1 + 5.39}{5.39} 2.9 - \frac{4.8}{5.39} = \underline{2.5^V}$$

finally

$$NM_H = V_{OH} - V_{IH} = 4.8 - 3.4 = 1.4^V$$

$$NM_L = V_{IL} - V_{OL} = 2.5 - 0 = \underline{2.5^V}$$

c)

$$\begin{aligned}
 C_{DB} &= WL_{diff} C_{jp} + (W + 2L_{diff}) C_{jswp} \\
 &= 22 \mu\text{m} \times 6 \mu\text{m} \times 0.3 \text{ FF}/\mu\text{m}^2 + (22 \mu\text{m} + 12 \mu\text{m}) \times 0.35 \text{ FF}/\mu\text{m} \\
 &= \underline{51.5 \text{ FF}}
 \end{aligned}$$

$$C_{Total} = (C_L \parallel C_{DB}) = C_L + C_{DB} = 100 + 51 = \underline{151 \text{ FF}}$$

$$t_{PLH} = RC_{Total} \ln(2) = 10^4 \times 151 \times 10^{-15} \ln(2) = \underline{1.05 \text{ nsec}}$$

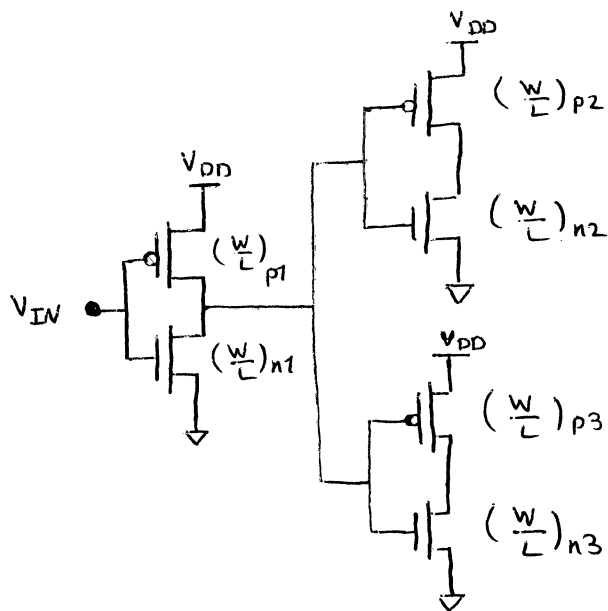
$$t_{PHL} = RC_{Total} \ln \left(\frac{-2 I_D R}{-2 I_D R - V_{DD}} \right) \quad \text{where } -I_D = 290 \mu\text{A} \quad \text{(from part (b))}$$

$$\Rightarrow t_{PHL} = 10^4 \times 151 \times 10^{-15} \ln \left(\frac{2 \times 290 \times 10^{-6} \times 10^4}{2 \times 290 \times 10^{-6} \times 10^4 - 5} \right) = \underline{2.99 \text{ nsec}}$$

d) Static power dissipation is due to the power consumed by the pull down resistor when V_{OUT} is high (V_{OH})

$$P_{diss} = \frac{V_{OH}^2}{R} = \frac{(4.8)^2}{10^4} = 2.3 \times 10^{-3} \text{ J/s}$$

3.



$$t_{ox} = 20 \text{ nm}$$

$$\Rightarrow C_{ox} = \frac{\epsilon_{ox}}{t_{ox}} = 0.17 \text{ fF}/\mu\text{m}^2$$

$$a) \quad V_M = \frac{V_{Tn} + \sqrt{\frac{k_p}{k_n}} (V_{DD} + V_{Tp})}{1 + \sqrt{\frac{k_p}{k_n}}}$$

$$\Rightarrow \frac{k_p}{k_n} = \left(\frac{V_M - V_{Tn}}{V_{DD} + V_{Tp} - V_M} \right)^2 = \left(\frac{2.5 - 0.7}{5 - 0.9 - 2.5} \right)^2 = 1.26$$

$$\frac{W_n}{W_p} = \frac{\mu_p}{\mu_n} \frac{k_n}{k_p} = \frac{200}{500} \frac{1}{1.26} = \underline{0.32}$$

$$b) \quad I_{Dn} = \left(\frac{W}{2L} \right)_n \mu_n C_{ox} (V_M - V_{Tn})^2 \Rightarrow$$

$$1 \text{ mA} = \frac{W_n}{2 \times 2 \mu\text{m}} 500 \times 0.17 \times 10^{-6} (2.5 - 0.7)^2 \Rightarrow \underline{W_n = 14.5 \mu\text{m}}$$

$$-I_{Dp} = \left(\frac{W}{2L} \right)_p \mu_p C_{ox} (V_{DD} - V_M + V_{Tp})^2 \Rightarrow$$

$$1 \text{ mA} = \frac{W_p}{2 \times 2 \mu\text{m}} 200 \times 0.17 \times 10^{-6} (5 - 2.5 - 0.9)^2 \Rightarrow \underline{W_p = 46.0 \mu\text{m}}$$

$$\begin{aligned}
 c) \quad C_{DB} &= W_n L_{diff_n} C_{j_n} + (W_n + 2L_{diff_n}) C_{JSW_n} + W_p L_{diff_p} C_{j_p} + (W_p + 2L_{diff_p}) C_{JSW_p} \\
 &= 14.5 \mu\text{m} \times 6 \mu\text{m} \times 0.1 \text{ FF}/\mu\text{m}^2 + (14.5 \mu\text{m} + 12 \mu\text{m}) 0.5 \text{ FF}/\mu\text{m} \\
 &\quad + 46.0 \mu\text{m} \times 6 \mu\text{m} \times 0.3 \text{ FF}/\mu\text{m}^2 + (46.0 \mu\text{m} + 12 \mu\text{m}) 0.35 \text{ FF}/\mu\text{m} \\
 &= \boxed{125 \text{ FF}}
 \end{aligned}$$

d) Since the source acting as ground for the four nMOS and pMOS in the second stage :

$$\begin{aligned}
 C_L &= 2 C_{gs_n} + 2 C_{gs_p} \approx 2 \left(\frac{2}{3} W_n L C_{ox} + \frac{2}{3} W_p L C_{ox} \right) \\
 &= 2 \left(\frac{2}{3} \times 14.5 \mu\text{m} \times 2 \mu\text{m} \times 0.17 \frac{\text{MF}}{\text{cm}^2} + \frac{2}{3} \times 46.0 \mu\text{m} \times 2 \mu\text{m} \times 0.17 \frac{\text{MF}}{\text{cm}^2} \right) \\
 &= \boxed{274 \text{ FF}}
 \end{aligned}$$

$$\begin{aligned}
 e) \quad t_{PLH} &\approx \frac{C_{total} V_{DD}}{\frac{W_p}{L_p} \mu_p C_{ox} (V_{DD} + V_{Tp})^2} = \frac{(125 \text{ FF} + 274 \text{ FF}) 5\text{V}}{\frac{46}{2} 200 \times 0.17 \times 10^{-6} (5 - 0.9)^2} \\
 &= \boxed{152 \text{ psec}}
 \end{aligned}$$

$$\begin{aligned}
 t_{PHL} &\approx \frac{C_{total} V_{DD}}{\frac{W_n}{L_n} \mu_n C_{ox} (V_{DD} - V_{Tn})^2} = \frac{(125 \text{ FF} + 274 \text{ FF}) 5\text{V}}{\frac{14.5}{2} 500 \times 0.17 \times 10^{-6} (5 - 0.7)^2} \\
 &= \boxed{175 \text{ psec}}
 \end{aligned}$$

4.

a) The graph for transistor output characteristics is on next page.

b) For small V_{DS} and $V_{BS} = 0$:

$$I_D = \frac{W}{L} \mu_n C_{ox} \left(V_{GS} - V_T - \frac{V_{DS}}{2} \right) V_{DS} \approx \frac{W}{L} KP (V_{GS} - V_{T0n}) V_{DS}$$

Therefore KP can be calculated from the slope of the graph in part (a) for the small V_{DS} region.

For high V_{DS} and $V_{BS} = 0$:

$$\begin{aligned} I_D &= \frac{W}{2L} \mu_n C_{ox} (V_{GS} - V_T)^2 (1 + \lambda V_{DS}) \\ &= \left[\frac{W}{2L} KP (V_{GS} - V_{T0})^2 \right] + \left[\frac{W}{2L} KP (V_{GS} - V_{T0})^2 \lambda \right] V_{DS} \end{aligned}$$

Therefore $LAMBDA$ can be calculated from the slope of the graph in part (a) for high V_{DS} region.

summary of results:

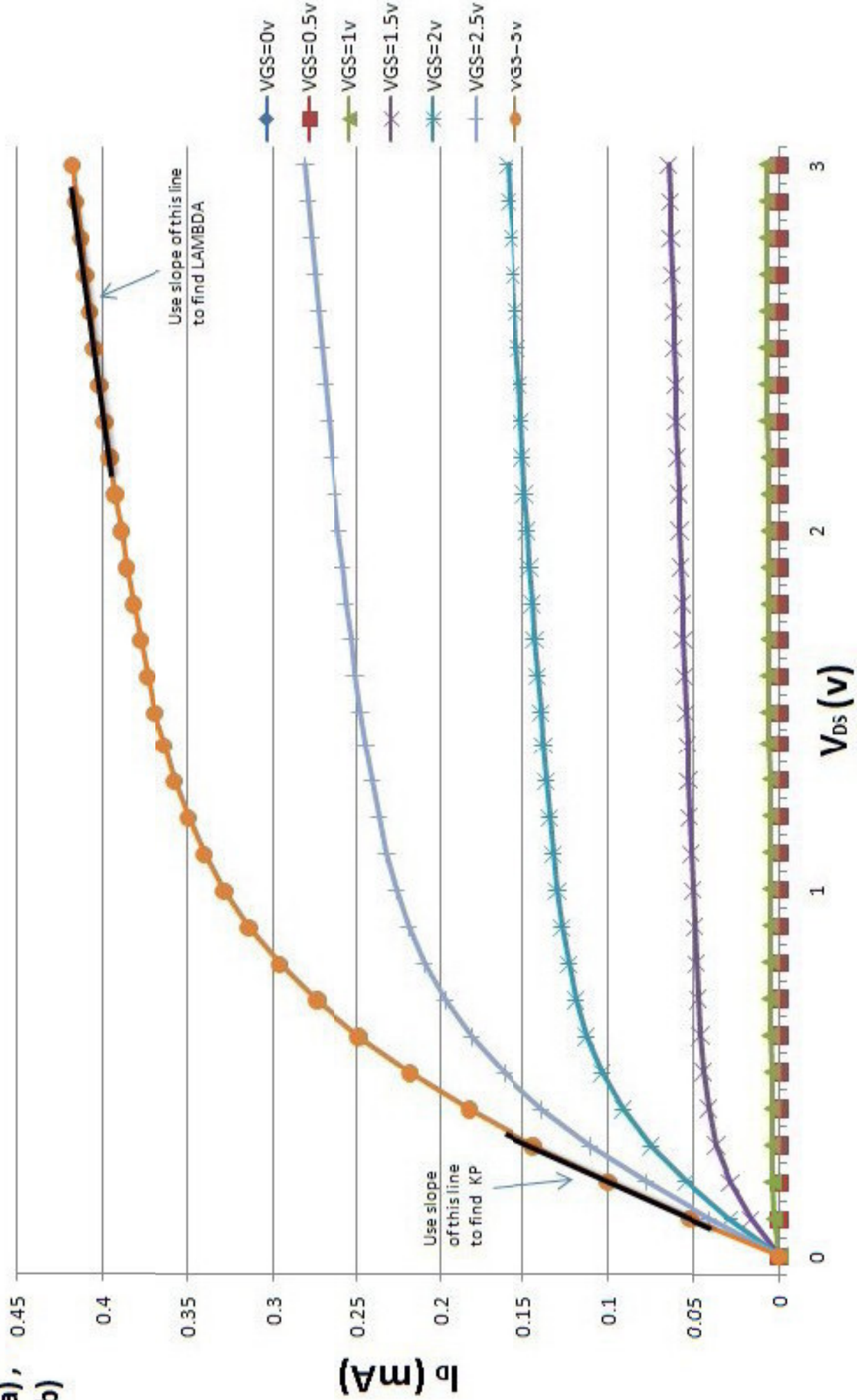
$$KP = 33.5 \frac{\mu A}{V^2}, \quad LAMBDA = 0.058 V^{-1}$$

From pset #5

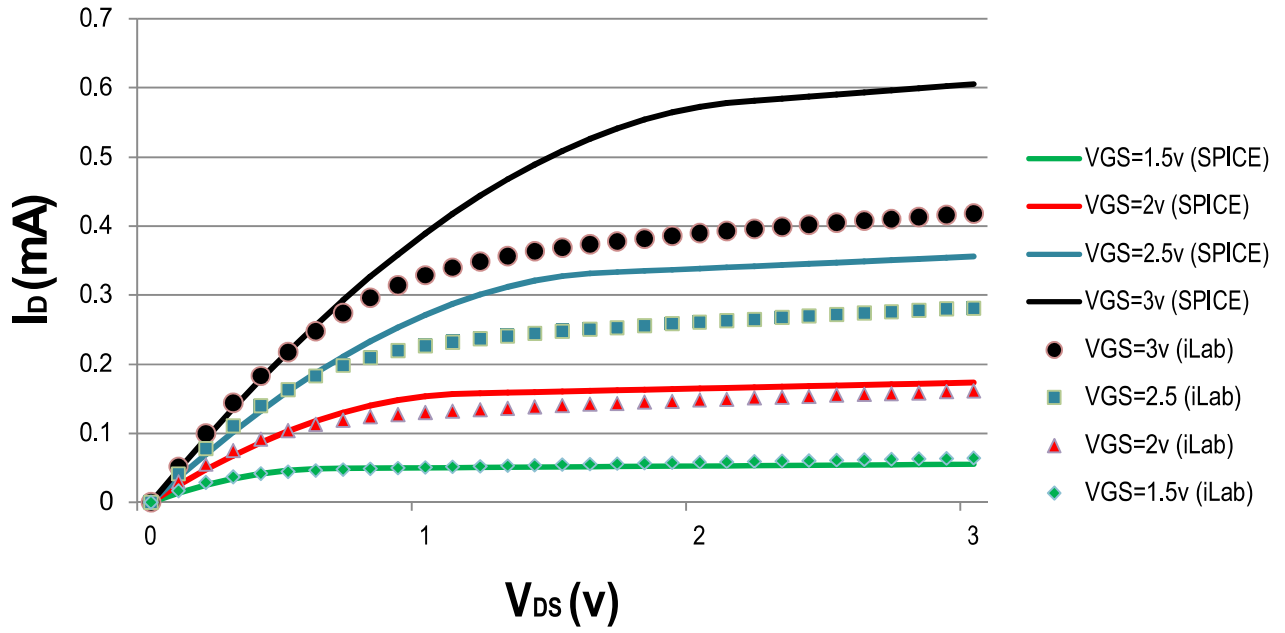
$$\rightarrow V_{T0} = 0.85 V, \quad GAMMA = 1.6 V^{1/2}, \quad PHI = 0.8 V$$

c) Output characteristics (I_D vs V_{DS}) and transfer characteristics (I_D vs V_{GS}) is on next pages.

4(a),
4(b)



4(c)



4(c)

