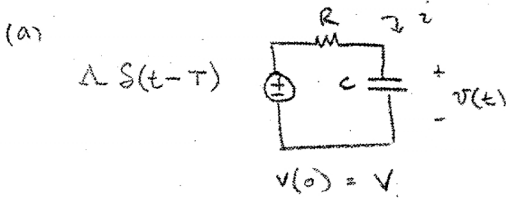


Exercise 7.1:



Impulses will give initial states, ignore in KVL.

$$iR + v(t) = 0$$

$$RC \frac{dv}{dt} + v(t) = 0$$



$$\frac{dv}{dt} + \frac{v}{RC} = 0 \Rightarrow v(t) = A e^{-t/RC}$$

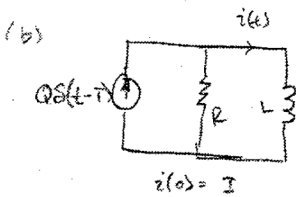
Two conditions:

① @  $t=0$ ;  $v(0) = V \Rightarrow v_1(t) = V e^{-t/RC}$   $t > 0$

② @  $t=T$ ;  $v(T) = \frac{\Lambda}{RC} \Rightarrow v_2(t) = \frac{\Lambda}{RC} e^{-(t-T)/RC}$   $t > T$

Using superposition:

$$v(t) = \begin{cases} V e^{-t/RC} & 0 \leq t < T \\ V e^{-t/RC} + \frac{\Lambda}{RC} e^{-(t-T)/RC} & t \geq T \end{cases}$$



KCL:  $\frac{v}{R} + i(t) = 0$

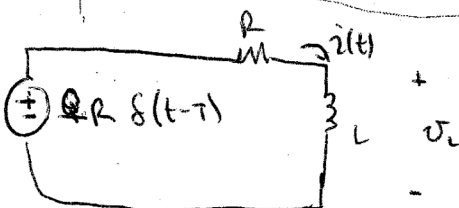
$$\frac{L}{R} \frac{di}{dt} + i = 0 \Rightarrow i(t) = A e^{-tR/L}$$

IC's

① @  $t=0$ ,  $i(0) = I \Rightarrow i_1(t) = I e^{-tR/L}$

② @  $t=T$ ,  $i(T) = \frac{RQ}{L} \Rightarrow i_2(t) = \frac{RQ}{L} e^{-(t-T)R/L}$

$$\Rightarrow i(t) = \begin{cases} I e^{-tR/L} & 0 \leq t < T \\ I e^{-tR/L} + \frac{RQ}{L} e^{-(t-T)R/L} & t \geq T \end{cases}$$



Exercise 7.2

$$\tau = \frac{L}{R}$$

At  $t < 0$ , the inductor is a short

At  $t = 0^-$  the inductor discharges through the resistor with time constant  $\frac{L}{R}$

$$\text{At } t = 0 \quad V = 1V$$

$$\text{At } t = 1\mu s \quad V \approx e^{-1} V$$

$$\frac{L}{R} = 1 \times 10^{-6}$$

$$L = 1 \times 10^{-6} \cdot R$$

At  $t = 0^+$

$$V = 1V = 1 \times 10^{-3} \times R$$

$$R = 1 \text{ k}\Omega$$

$$L = 1 \text{ mH}$$

### Problem 7.1

- (A) In DC, the capacitor  $C$  will be an open,  
the inductor  $L$  in the transformer will be a short.

No voltage from  $v_{IN}$  will be seen at the gate of the MOSFET.

$$V_{GS} = \frac{R_2}{R_1 + R_2} \cdot V_S$$

$$I_D = \frac{K}{2} (V_{GS} - V_T)^2 = \frac{K}{2} \left( \frac{R_2}{R_1 + R_2} V_S - V_T \right)^2$$

Since  $L$  is a short;  $v_o = 0$ .

$$\therefore V_{out} = 0$$

- (B) No, a bias at  $v_{IN}$  will not be useful since the capacitor will block DC voltage. The MOSFET is biased by  $R_1$  &  $R_2$ .

Since  $V_{out} = 0$ , there is no large signal to remove from the output.

- (C) In DC:

$$V_{GS} = V_S$$

for saturation,  $v_{DS} > v_{GS} - V_T$ .

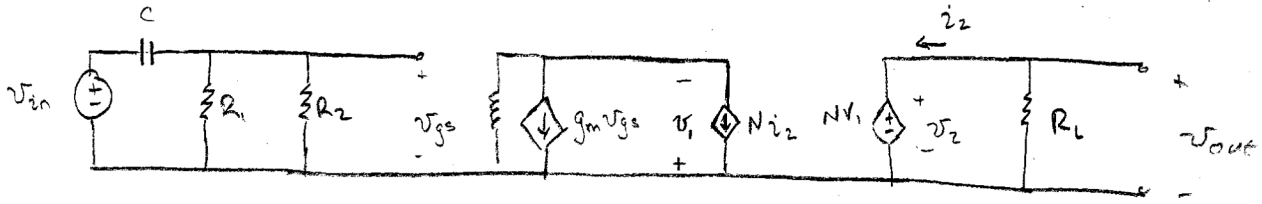
This will always be true.  $V_{GS}$  needs to be greater than  $V_T$

$$V_{GS} > V_T$$
$$\frac{R_2}{R_1 + R_2} V_S > V_T$$

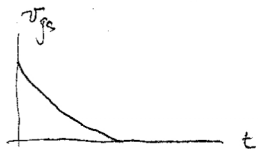
$$\frac{R_2}{R_1} > \frac{V_T/V_S}{1 - V_T/V_S}$$

Assume that in small signal:

- 1) the capacitor is a short
- 2) the inductor is an open

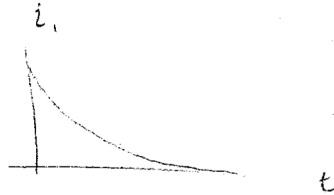


The capacitor C will cause the  $v_{gs}$  to decay

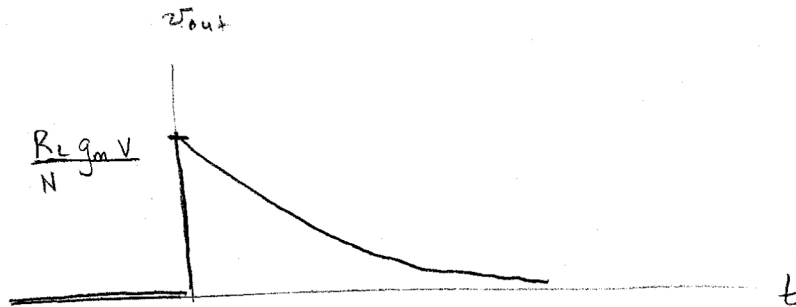


The inductor will cause the current  $i_2$  to decay as well

to a step in current ( $g_m v_{gs}$ )



Therefore, to a step the output will contain two time constants



To a step input:

$$v_{gs} = V e^{-t/\tau}$$

$$\tau_1 = (R_1 // R_2) C$$

$$i_d = \underbrace{K(V_{GS} - V_T)}_{g_m} \cdot v_{gs}$$

$$i_d = V g_m e^{-t/\tau_1}$$

$$i_1 = \frac{v_{out}}{N}$$

$$i_2 = -\frac{v_{out}}{R_L}$$

$$i_3 = -\frac{v_{out} \cdot N}{R_L}$$

Using KCL above the MOSFET:

$$-i_1 + i_2 - i_d = 0$$

$$+\frac{v_{out} N}{R_L} + i_2 - V g_m e^{-t/\tau_1} = 0$$

$$\frac{dv_{out}}{dt} + \frac{R_L}{LN} v_{out} + \frac{V g_m}{\tau_1} e^{-t/\tau_1} = 0$$

$$v_{out, hom} = A e^{-t/\tau_2}$$

$$A = \frac{V g_m}{N} \cdot R_L \quad \text{initial jump in } v_{out}$$

$$\tau_2 = \frac{LN}{R_L}$$

$$v_{out, part} = \frac{-V g_m / \tau_1}{\frac{R_L}{LN} - 1/\tau_1} e^{-t/\tau_1} = \frac{-V g_m LN}{R_L \tau_1 - LN} e^{-t/\tau_1}$$

$$v_{out} = \frac{V g_m R_L}{N} e^{-t/\tau_2} - \frac{V g_m LN}{R_L \tau_1 - LN} e^{-t/\tau_1} \quad \tau_1 = (R_1 // R_2) C \quad \tau_2 = \frac{LN}{R_L}$$

(F) Notice that the two solutions have different time constants that will both be large.

$N$  is the number of turns around the transformer. Typically this is very large.

$$\tau_2 > \tau_1$$

The decay will be dominated by  $\tau_1$ .

(6)

## Problem 7.2

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(a) For the time constant,  $\tau$ , the initial slope of the rise & fall curves are  $\frac{1}{\tau}$ .

See attached graphs.

Pull-up

$$\frac{1}{\tau_{pu}} = \frac{-1.394 - -2.298}{51 \text{ ns} - 50 \text{ ns}}$$

$$\tau_{pu} = 1.1 \text{ ms}$$

Pull-down

$$\frac{1}{\tau_{pd}} = \frac{2.138 - -2.460}{1 \text{ ms}}$$

$$\tau_{pd} = 0.22 \text{ ms}$$

(b) Offset of  $-75 \text{ mV}$  was given to achieve output offset of  $-180 \text{ mV}$ .

Pull-up

$$\frac{1}{\tau_{pu}} = \frac{-1.133 - -1.806}{1 \text{ ms}}$$

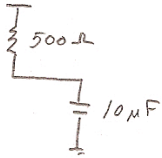
$$\tau_{pu} = 1.5 \text{ ms}$$

Pull-down

$$\frac{1}{\tau_{pd}} = \frac{1.636 - 0.8698}{1 \text{ ms}}$$

$$\tau_{pd} = 1.3 \text{ ms}$$

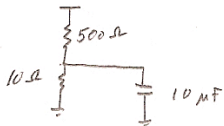
(c) For Pull-up: MOSFET is off



$$\tau = RC = (500 \Omega)(10 \mu\text{F})$$

$$\tau_{pu} = 5 \text{ ms}$$

For Pull-down: MOSFET is on



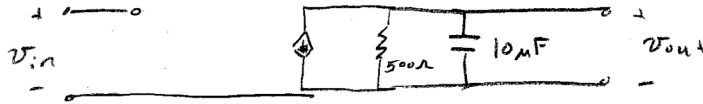
$$\tau = RC = \frac{(500 \Omega)(10 \Omega)}{(510 \Omega)} \approx 10 \mu\text{F}$$

$$\tau_{pd} = 0.1 \text{ ms}$$

Discrepancies can arise from the estimation of the initial slope. Device tolerances and the estimation  $R_{on}$  also have an effect on the measured value.

(D) Small signal model:

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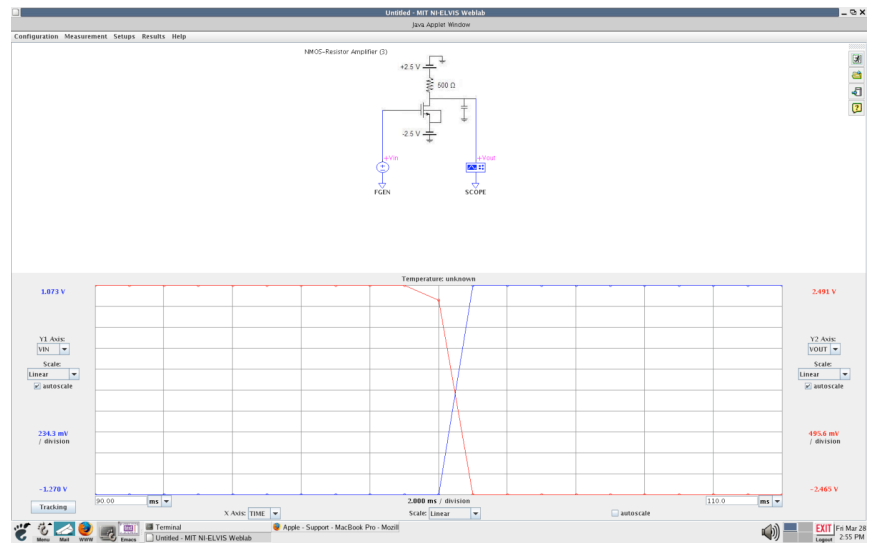
The resistance looking from  $V_{out}$  is just  $500\Omega$

$$\tau = (500\Omega)(10\mu F)$$

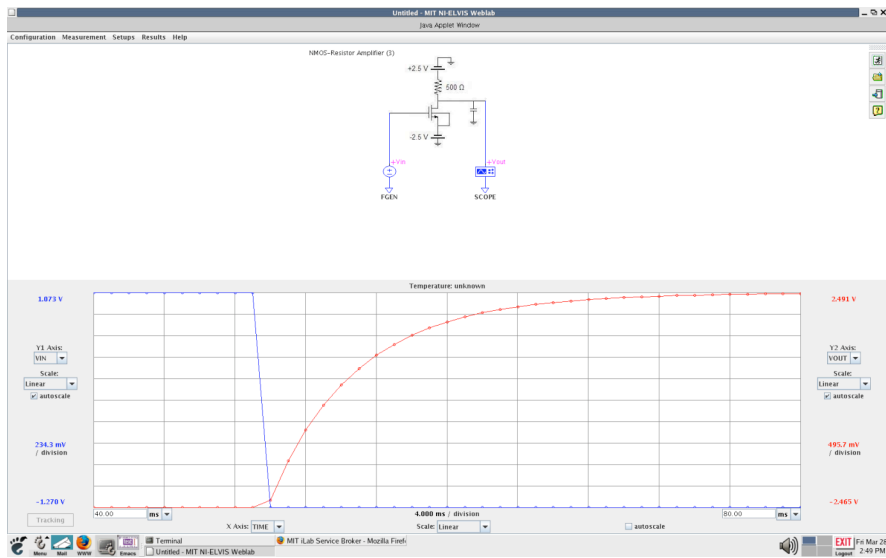
$$\tau = 5\text{ms}$$

Note: for the small signal there is no difference between pull-up and pull-down. Therefore the time constants should be the same.

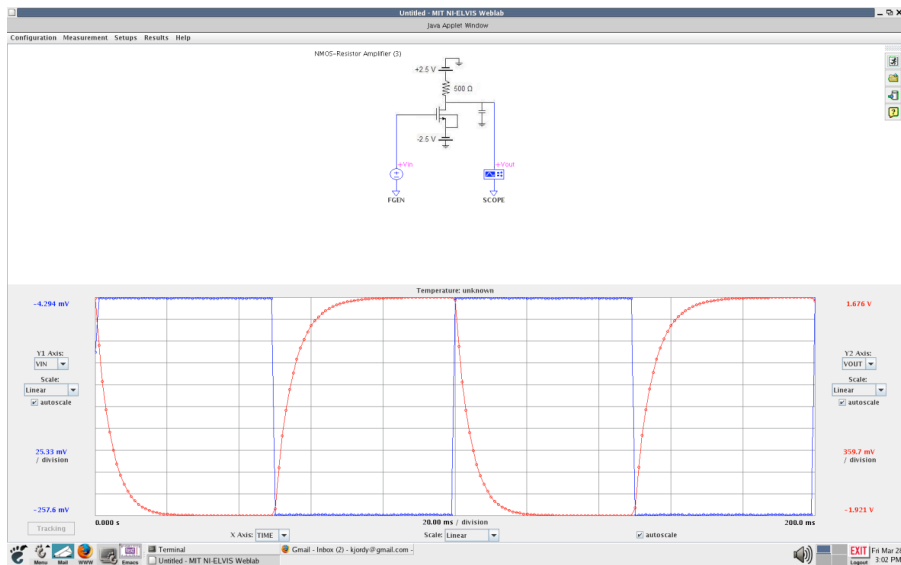




Part A: Pull-down



Part A: Pull-up



Part B

### Problem 7.3

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(a) Calculate power for each combination.

$$P = \frac{V^2}{R}$$

$$\underline{00}: P = \frac{V_s^2}{R_{pu} + R_{ow}} \approx \frac{V_s^2}{R_{pu}}$$

$$\underline{01}: P = \frac{V_s^2}{R_{pu} + R_{oz}} \approx \frac{V_s^2}{R_{pu}}$$

$$\underline{00}: P = \frac{V_s^2}{R_{pu}}$$

$$\underline{10}: P = \frac{V_s^2}{R_{pu}}$$

Note for:

$$R_{pu} + R_{ow} \approx R_{pu}$$

for  $R_{ow} \ll R_{pu}$

$$\bar{P} = \frac{V_s^2}{R_{pu}}$$

(b) Make the assumption that  $v_{g3}$  goes to zero when either  $M1$  or  $M2$  is on. Thus  $v_{g3}$  is either 0 or  $V_s$ .

In one cycle  $v_{g3}$  goes from  $L \rightarrow H$  and  $H \rightarrow L$  once.

From Lecture 12:

$$\text{Dissipation of } C_{gs3} = C_{gs} V_s^2 f = \frac{C_{gs} V_s^2}{4T}$$

$$\text{Dissipation of } C_{out} = \frac{N C_{gs} V_s^2}{4T}$$

$$\text{Total Dynamic Dissipation} = \frac{C_{gs} V_s^2}{4T} (N+1)$$

(b)  $\frac{\text{Static Loss}}{\text{Dynamic Loss}} = \frac{V_s^2 / R_{pu}}{\frac{C_{GS} V_s^2}{4T} (N+1)}$

(11)

$= \frac{5T}{C_{GS} R_{pu} (N+1)} > 0$

for  $T \gg C_{GS} R_{pu} \Rightarrow N$  not much larger than 1

Static Loss is greater

# Problem 7.4

(12)

$$\omega = 10^7 \text{ rad/s}$$

$$v_{\text{peak}} = 100 \text{ mV}$$

$$i_{\text{peak}} = 10 \text{ mA}$$

(A)  $\frac{1}{\omega} = \sqrt{LC}$

$$i_{\text{peak}} = v_{\text{peak}} \sqrt{\frac{C}{L}}$$

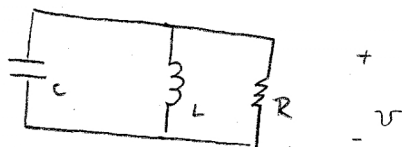
$$\begin{aligned} L &= 1 \text{ mH} \\ C &= 100 \text{ } \mu\text{F} \end{aligned}$$

(B) Total energy:

When  $i=0$  no energy in inductor.

$$E = \frac{1}{2} C v_{\text{pk}}^2$$

(C)



For Lecture:

$$v(t) = e^{-\alpha t} (\cos(\omega_0 t + \phi))$$

$$\alpha = \frac{1}{2RC}$$

$$\omega_0 = \sqrt{\frac{1}{LC}}$$

Power decays by  $e^{-\alpha t}$

$$\text{Time const} = \frac{1}{\alpha} = 2RC$$

$$2RC = \tau = 10 \text{ } \mu\text{s}$$

$$R = 5 \text{ m}\Omega$$