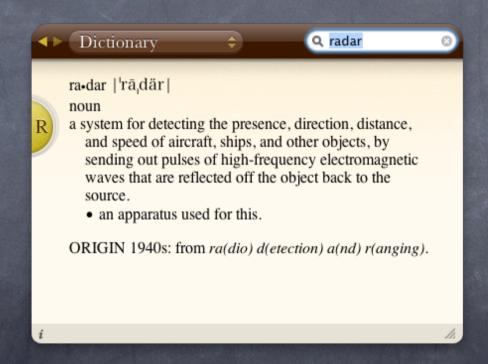
RADAR?

Thomas Ulich Sodankylä Geophysical Observatory Finland

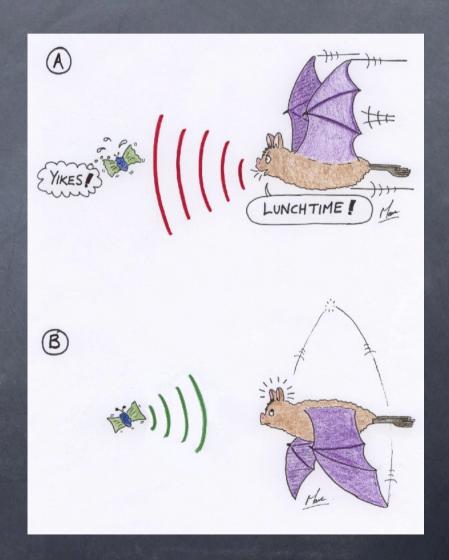
Radio Detection And Ranging

RADAR



Nature's done it already





Hans Christian Ørsted

On 21st April 1820, Ørsted discovered a direct relationship between electricity and magnetism, which prompted much research into electrodynamics.



(14 August 1777 - 9 March 1851)

André-Marie Ampère

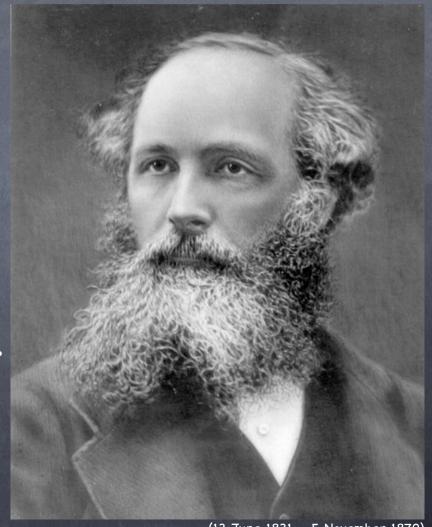
Inspired by Ørsteds
discovery, Ampère
developed a mathematical
theory describing
electromagnetic
phenomena and predicting
many new ones.



(20th January 1775 - 10th June 1836)

James Clerk Maxwell

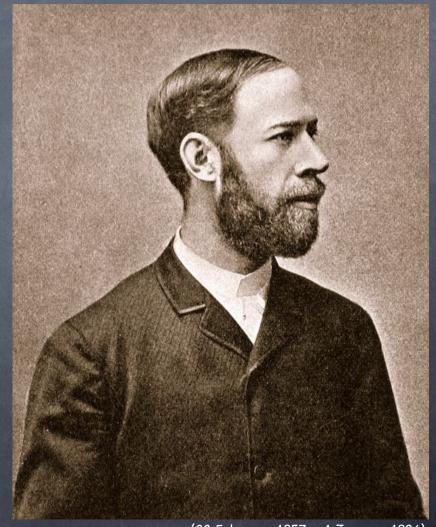
The Maxwell Equations showed that electricity and magnetism are two aspects of the same force.



(13 June 1831 – 5 November 1879)

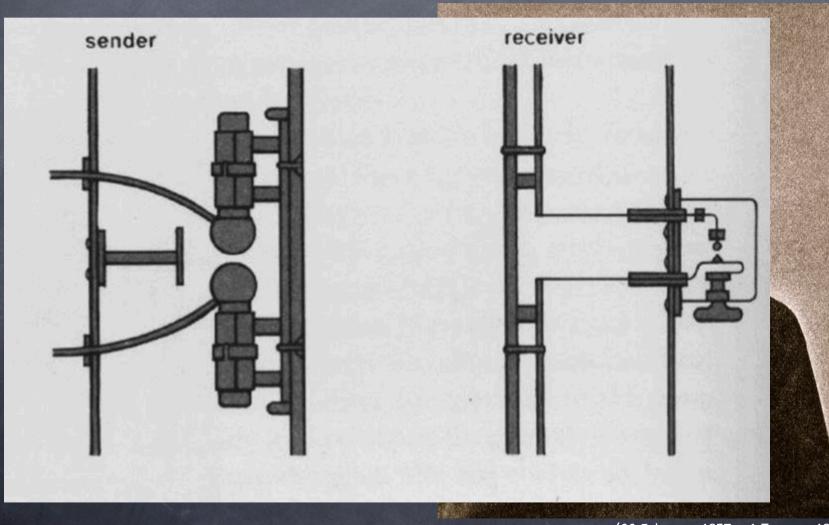
Heinrich Rudolf Hertz

Hertz proved that electricity can be transmitted by electromagnetic waves.



(22 February 1857 - 1 January 1894)

Heinrich Rudolf Hertz



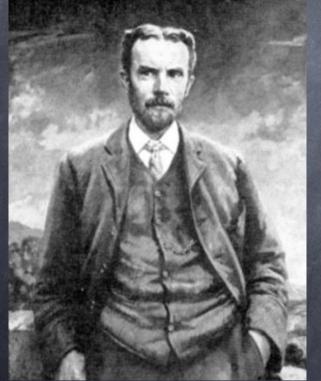
Guglielmo Marconi

Inventor of the radio telegraph system; first transatlantic radio transmission on 12 December 1901 at 820 kHz.



Ionised Layer

Oliver Heaviside



(18 May 1850 - 3 February 1925)

Arthur E Kennelly

In 1902, Heaviside and Kennelly independently predicted an ionised layer in the upper atmosphere that would reflect radio waves.



(17 December 1861 - 18 June 1939)

Edward Appleton

Appleton and his colleagues were one of two teams to prove the existence of a reflecting layer at a height of about 100 km (E layer), soon followed by the discovery of the F layer at around 250 km.

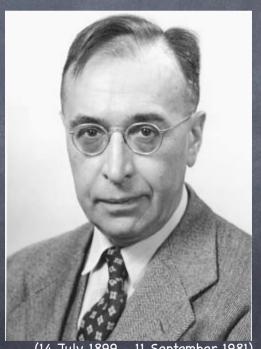


(6 September 1892 - 21 April 1965)

Ionosonde

G Breit and M A Tuve, A radio method of estimating the height of the conducting layer, Nature, 116, p. 357, 1925.

Gregory Breit Merle Tuve

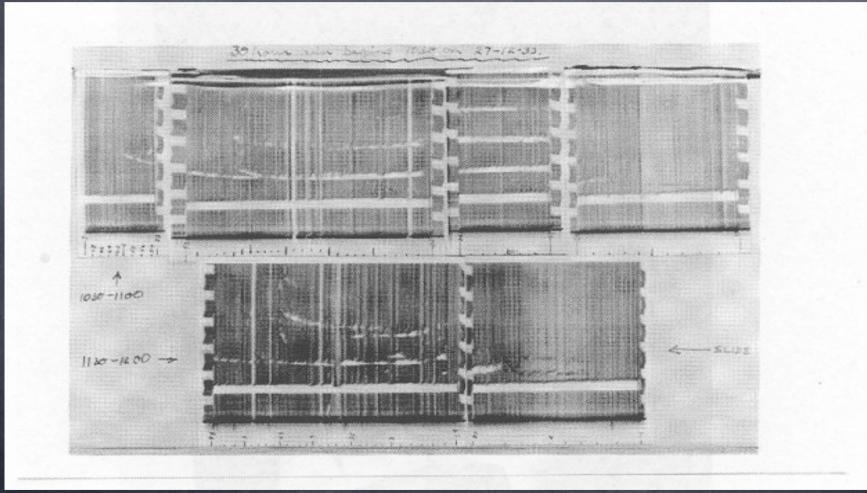


(14 July 1899 - 11 September 1981)



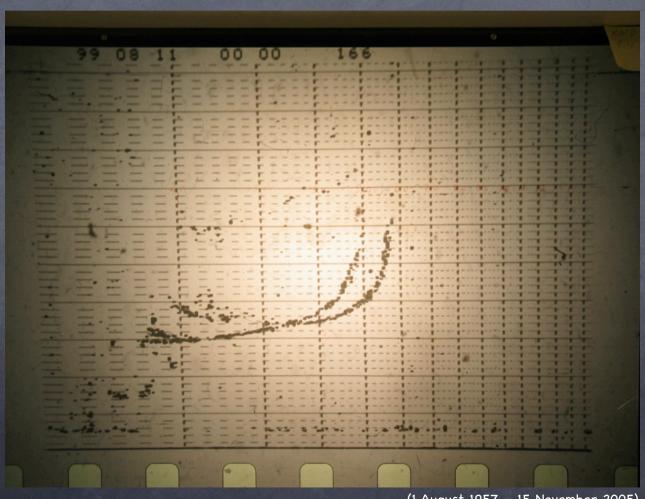
(27 June 1901 - 20 May 1982)

Regular Ionograms



Radio Research Station Slough, Buckinghamshire 27th December 1933, 10:30–11:00 UTC and 11:30–12:00 UTC.

Sodankylä Ionosonde



(1 August 1957 - 15 November 2005)

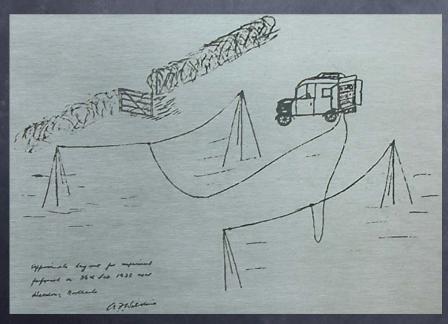
Detecting Aircraft



Denge, Dungeness, Kent, UK

Robert Watson-Watt

Daventry Experiment on 26 Feb. 1935; patent for RADAR on 2 Apr.; by June detecting aircraft at 27 km.

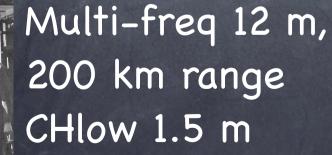


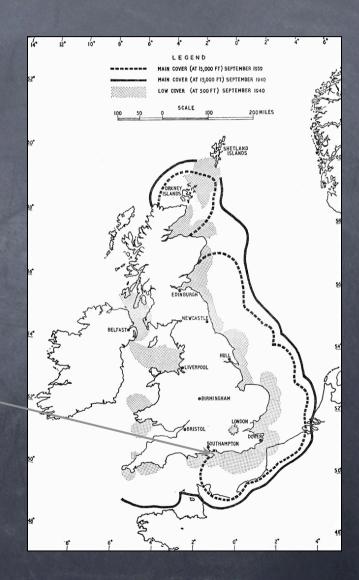


(13 April 1892 - 5 December 1973)

Chain Home

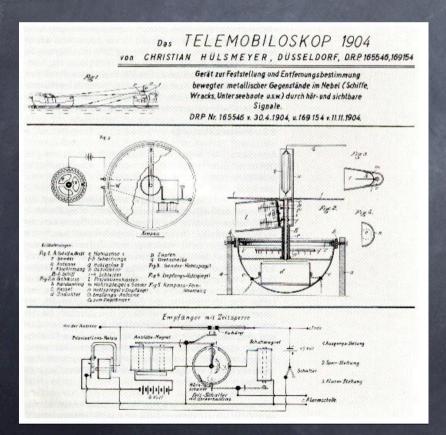


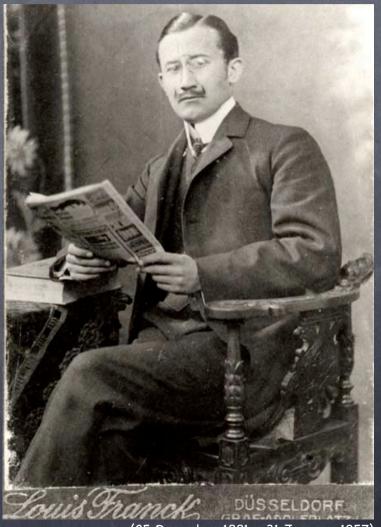




Christian Hülsmeyer

Invented RADAR ...
... but no-one noticed.

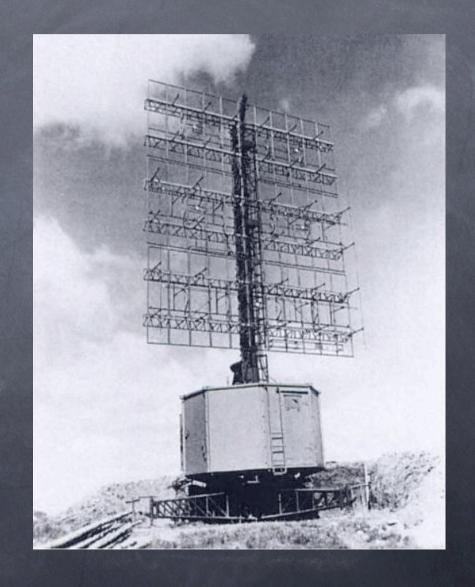




(25 December 1881 - 31 January 1957)

Freya

- German radar op. 1938.
- ▶ Portable(ish).
- ▶ 120-130 MHz (2.5-2.3 m).
- PRF 500 Hz, 3 µs pulses.
- Rotates 360°, 160 km range.
- Countermeasures:
 - Moonshine: re-emit amplified pulses (8 a/c = 100 bombers).
 - ▶ Jamming: 9 a/c create a 200-mile (320 km) gap.



September 1939

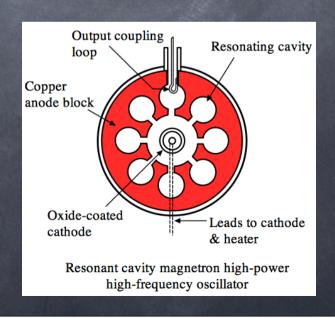
More or less rudimentary but operational radars:

Britain, France, Germany, Hungary, Italy, Japan, the Netherlands, Russia, Switzerland, and the USA.

Cavity Magnetron

- *Invented at U Birmingham, UK, by John Randall and Henry Boot.
- *By mid-1940 cavity magnetron developed into a small, light-weight transmitter (3 GHz at 15kW).
- ◆10x improvement over other radar.





Status after WWII

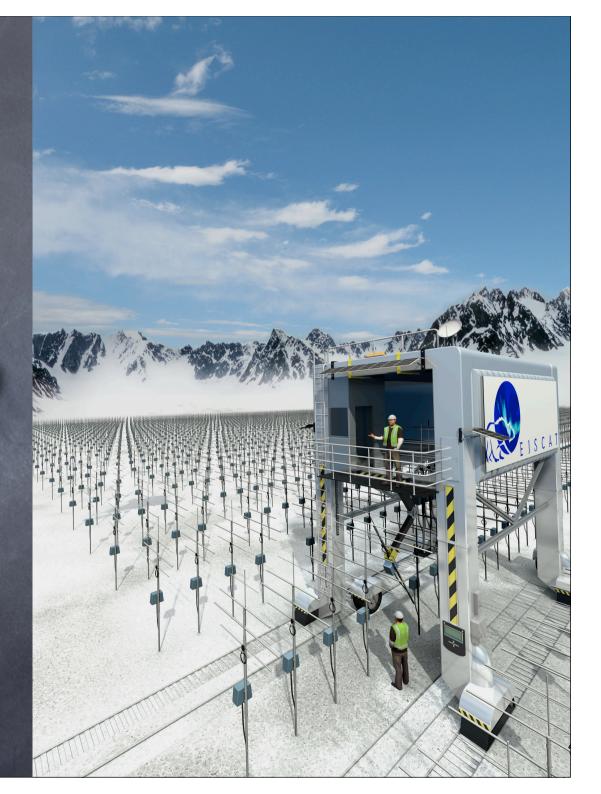
- RADAR had evolved from prototypes to a multitude of different systems.
- Microwave signal generation had become practical.
- * Advances in aerials, transmitters, receivers, displays etc. led to wide-spread use in communications and radar applications.

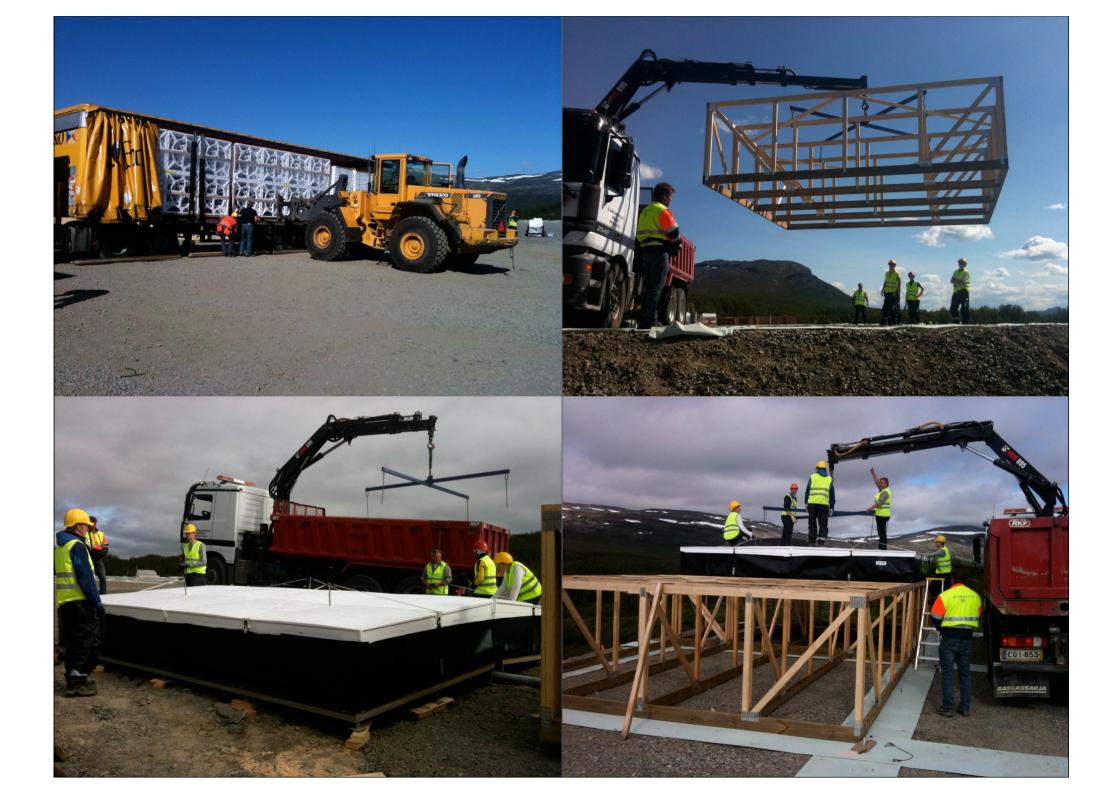
... fast forward ...

Does the Future of Incoherent Scatter look like this?

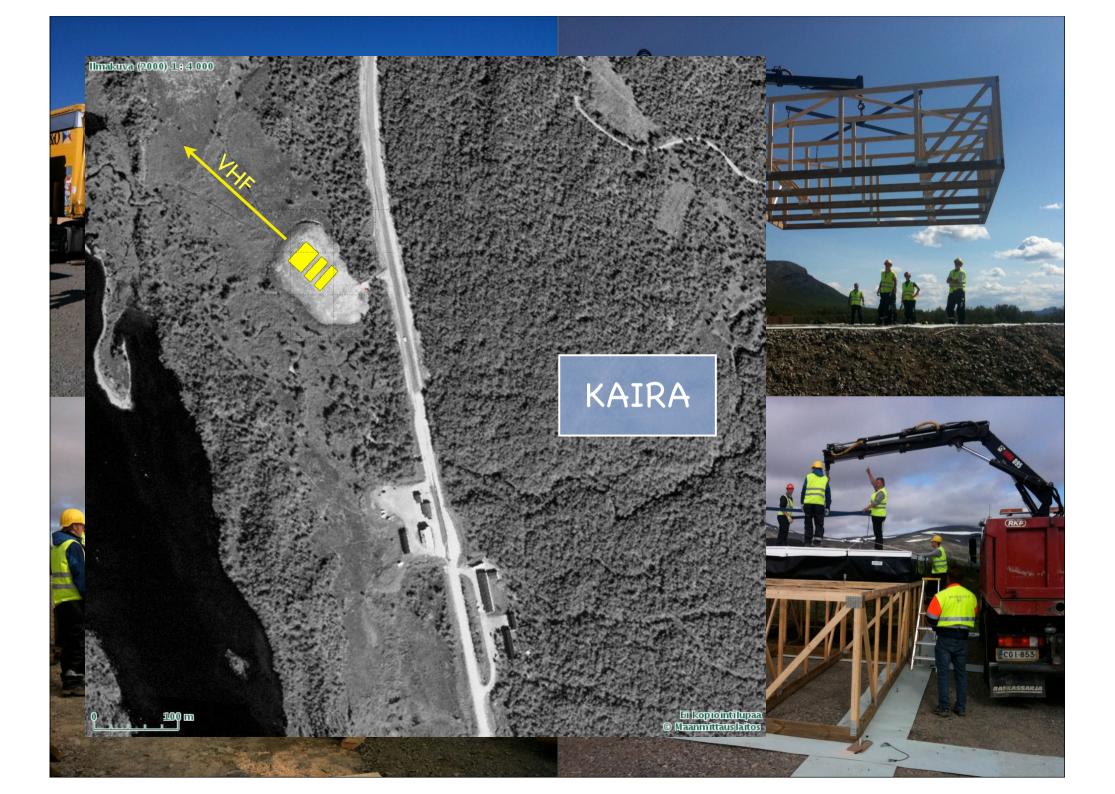
EISCAT_3D

Welcome aboard!









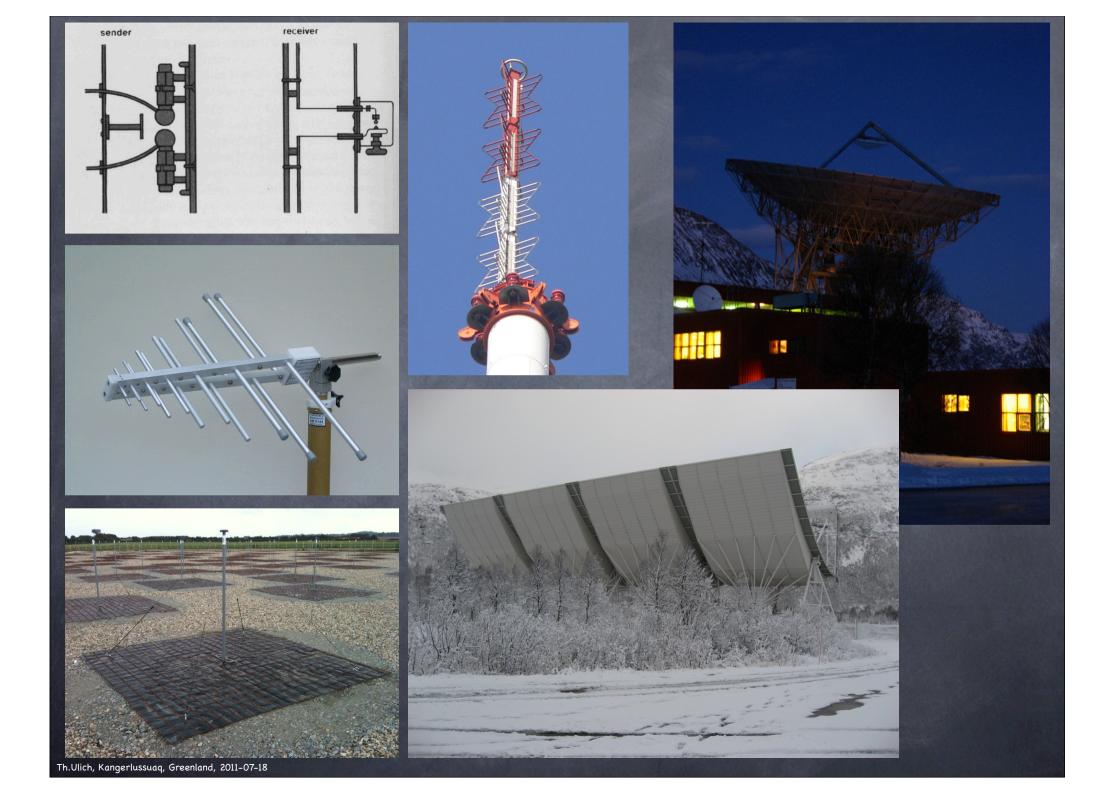
30-300 GHz / 10-1 mm	EHF	microwave radio relays		
3-30 GHz / 10-1 cm	SHF	satellite comm & nav, wireless LAN	weather radars	
0.3-3 GHz / 1-0.1 m	UHF	cell phones, TV, microwave ovens	EISCAT UHF, ESR, AMISR	
30-300 MHz / 10-1 m	VHF	FM radio, TV, HAM	EISCAT VHF, JRO, MST radars, meteor radars	
3-30 MHz / 100-10 m	HF	shortwave radio	Ionosondes, SuperDARN	
0.3-3 MHz / 1-0.1 km	MF	AM radio	Ionosondes	
30-300 kHz / 10-1 km	LF	radio beacons, submarine comm	AARDDVARK	
3-30 kHz / 100-10 km	VLF	navigation	AARDDVARK	
0.3-3 kHz / 1-0.1 Mm	ULF	audio signals on analogue telephone		
30-300 Hz / 10-1 Mm	SLF	electric grids		
3-30 Hz / 100-10 Mm	ELF	metal detectors	Earth-iono. waveguide, Schumann resonance	

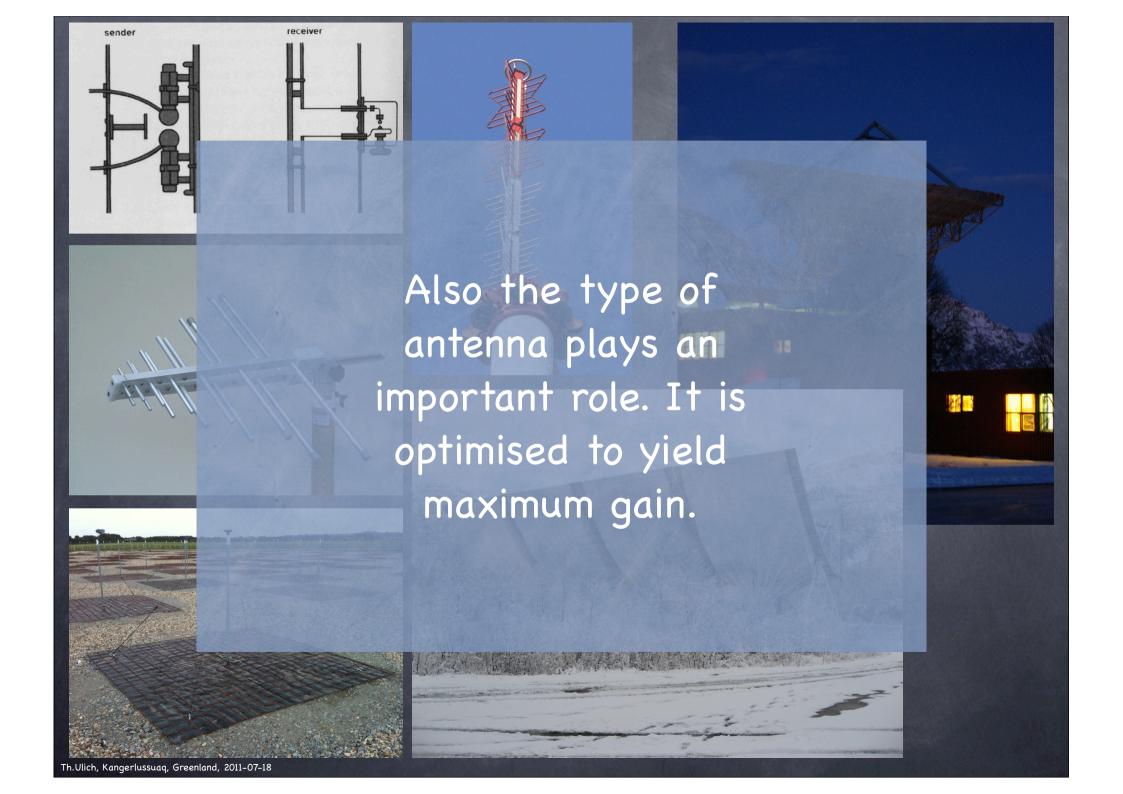
Туре	Frequency	λ [m]	Power [kW]	Aperture [λ]	Height
MF Radar	MF-HF	150-50	0.01-1	1–10	M, L, T, I
Ionosonde	HF	300-10	0.01-5	0.5-1	т, І
Coherent scatter rad	HF-VHF	30-1	0.1-1	5-50	Т, І
Meteor radar	HF-VHF	10-6	0.1–10	2-10	M, L, T
MST radar	VHF	6-7	1–100	5-50	M, S, T
Incoherent scatter rad	VHF-UHF	6-0.25	500-2000	100-300	M, L, T, I
ST radar	UHF	6-0.1	1–500	10-500	S, T

Туре	Frequency	λ [m]	Power [kW]	Aperture [λ]	Heigh†
MF Radar					M, L, T, I
Ionosonde	What	300-10 You Co	o.01-5 In obset	0.5-1 °Ve is	T, I
Coherent scatter rad		ESTATION OF THE PARTY OF THE PA	f frequ		T, I
Meteor radar	H(wave		, power	and	M, L, T
MST radar		aper 6-7	ture!		M, S, T
Incoherent scatter rad	VHF-UHF				M, L, T, I
ST radar	UHF	6-0.1	1–500	10-500	S, T

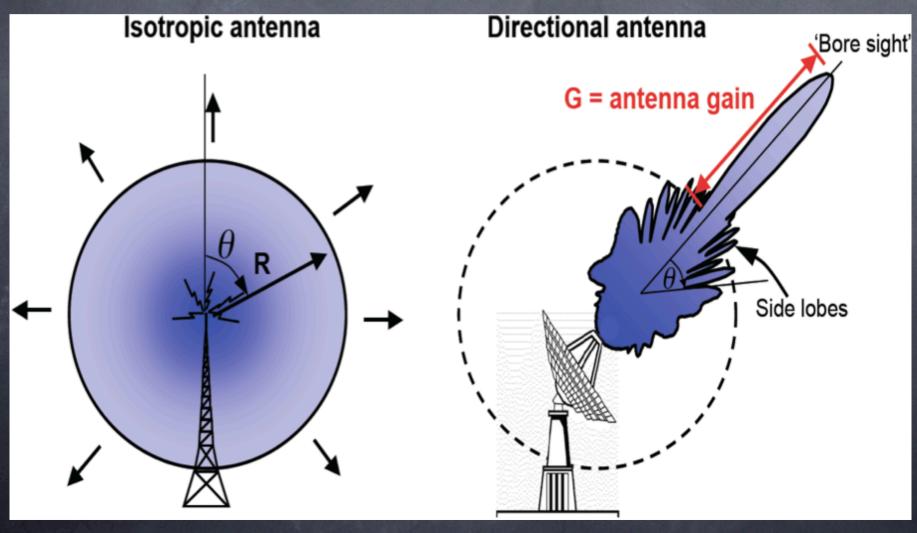
Far-Field Condition

- Far-field of antenna: electromagnetic waves can be approxmated by plane waves.
- Energy distribution is well defined.
- Most atmospheric radars are designed to operate in the far-field, farther away than $D_a^2/λ$.
- \odot EISCAT UHF: $(32m)^2 / 0.32m = 3200m$
- \odot MU radar: $(103\text{m})^2 / 6.45\text{m} = 1600\text{m}$





Radiation Patterns



Radar Equation

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \cdot \frac{1}{4\pi R^2} \cdot A$$

Received power

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \cdot \frac{1}{4\pi R^2} \cdot A$$

Received power is equal to - transmitted power ...

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \cdot \frac{1}{4\pi R^2} \cdot A$$

- transmitted power times
- transmitter gain ...

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \left(\frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \cdot \frac{1}{4\pi R^2} \cdot A \right)$$

- transmitted power times
- transmitter gain times
- spread factor at transmitter ...

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \cdot \frac{1}{4\pi R^2} \cdot A$$

- transmitted power times
- transmitter gain times
- spread factor at transmitter times
- any losses in the system ...

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \left\{ \sigma \right\} \cdot \frac{1}{4\pi R^2} \cdot A$$

- transmitted power times
- transmitter gain times
- spread factor at transmitter times
- any losses in the system times
- backscatter cross section ...

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \left(\frac{1}{4\pi R^2}\right) \cdot A$$

- transmitted power times
- transmitter gain times
- spread factor times
- any losses in the system times
- backscatter cross section times
- spread factor at point target ...

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \cdot \frac{1}{4\pi R^2} \cdot A$$

- transmitted power times
- transmitter gain times
- spread factor times
- any losses in the system times
- backscatter cross section times
- spread factor at point target times
- receiver aperture.

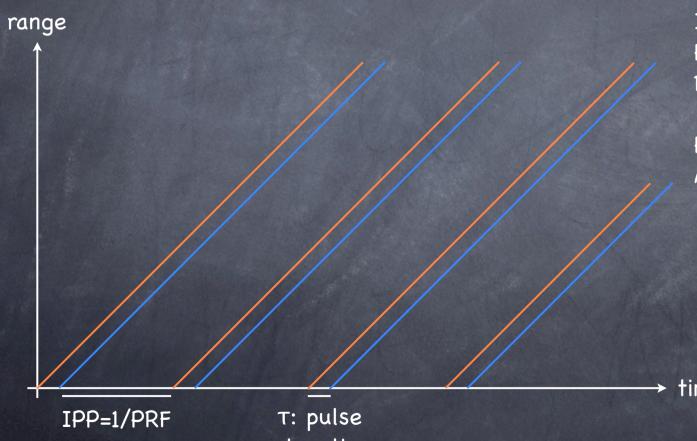
Hard vs Soft Target aka Point vs Volume Target

$$P_r = P_t \cdot \frac{4\pi A}{\lambda^2} \cdot \frac{1}{4\pi R^2} \cdot \frac{1}{L} \cdot \sigma \cdot \frac{1}{4\pi R^2} \cdot A$$

Received power is equal to

- transmitted power times
- transmitter gain times
- spread factor times
- any losses in the system times
- backscatter cross section times
- spread factor at point target times
- receiver aperture.

Integration over beamfilling scatter volume results in cancellation of the target spread factor.



IPP: Inter-pulse period

PRF: Pulse repetition freq

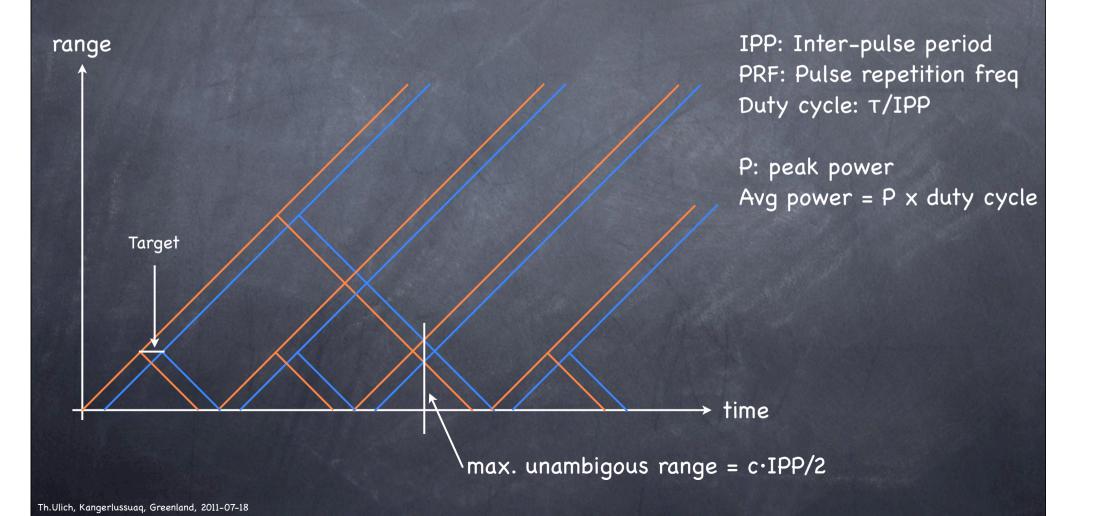
Duty cycle: T/IPP

P: peak power

Avg power = P x duty cycle

→ time

length





IPP: Inter-pulse period

PRF: Pulse repetition freq

Duty cycle: T/IPP

P: peak power

Avg power = P x duty cycle

→ time

Pulse coding



IPP: Inter-pulse period

PRF: Pulse repetition freq

Duty cycle: T/IPP

P: peak power

Avg power = P x duty cycle

Range resolution:

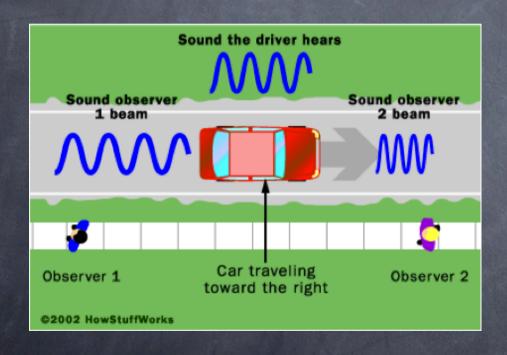
 $\Delta r = c \cdot \tau / 2$

1μs ⇔ 150m

→ time

Pulse length	Range resolution
1 ns	15 cm
10 ns	1.5 m
100 ns	15 m
1 µs	150 m
10 µs	1.5 km
100 µs	15 km
1 ms	150 km

Doppler Radar



Return from moving target:

$$cos(2\pi f_o(t+2R/c)) =$$
 $cos(2\pi (f_o+f_D)t)$
where
$$R = vt,$$

$$f_D = 2f_ov/c = 2v/\lambda_o$$

Resolving Doppler

- Tx signal: cos(2πf₀t)
- Toppler-shifted rx signal: $cos(2\pi(f_o+f_D)t)$
- Multiply by tx signal, low-pass filter => Doppler frequency $cos(2\pi f_D t)$
- Generate signal by mixing sin and cos using two oscillators 90° out of phase: $Aexp(i2\pi f_Dt) = cos(2\pi f_Dt) + isin(2\pi f_Dt) = I + iQ$
- Signed Doppler => signed radial velocity

Summary

- Pulse length => range resolution
- IPP => range ambiguity <=> time scale process
- Wavelength => scale of process/object
- Power, aperture, antenna design=> scatter cross section, received signal
- Aperture, wavelength => far-field distance