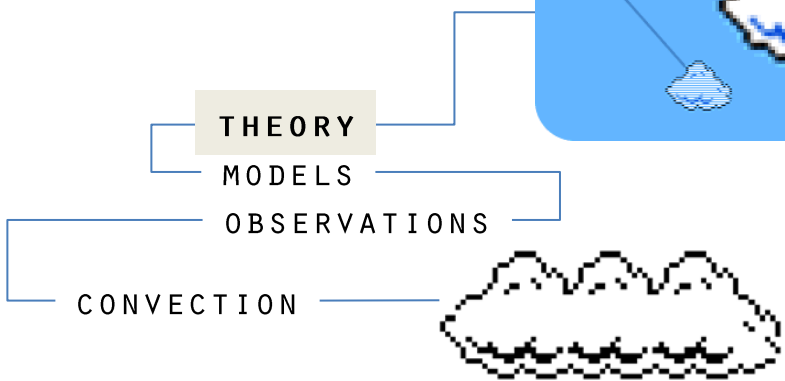



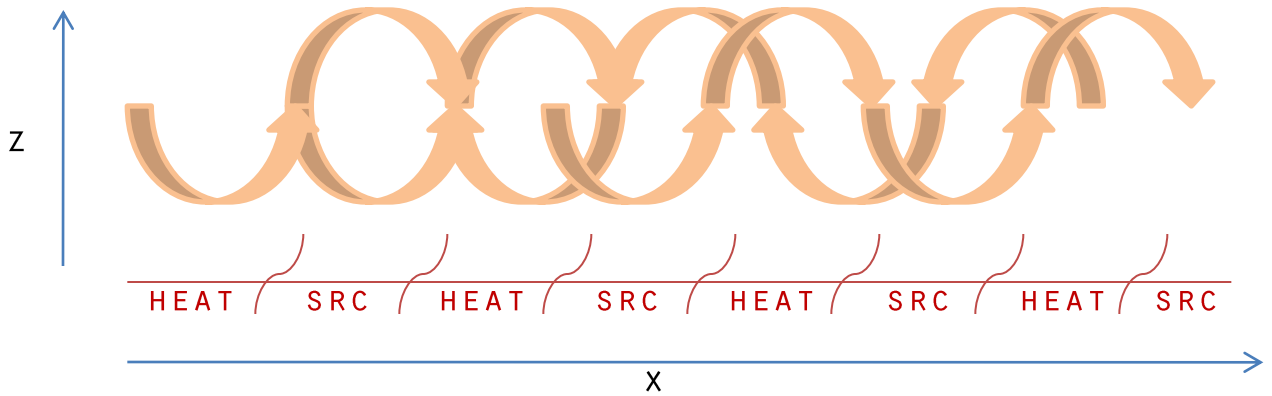


ENVIRONMENTS



-  **TANK:ONE** 2
-  **ATMOS:ONE** 3
-  **TANK:TWO** 1
-  **ATMOS:TWO** 4

WHAT IS THE NATURE OF THE CONVECTIVE PROCESS?

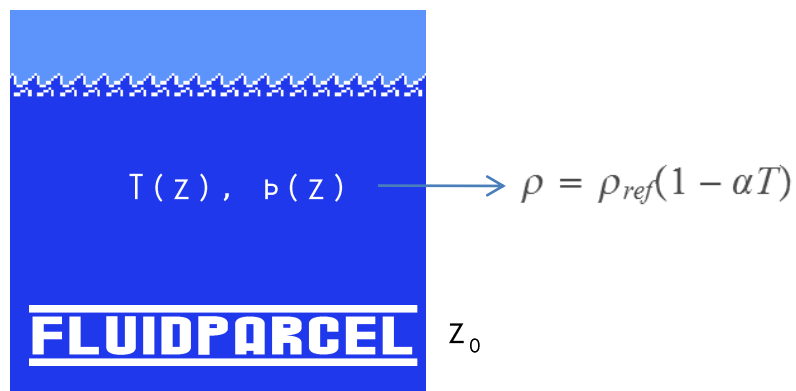


OVERTURNING OF A FLUID
(X-SCALING DEPENDENT ON UNSTABLE LAYER'S Z-DEPTH!)

TWO MEDIUMS FOR THE CONVECTIVE PROCESS

FIRST: *INCOMPRESSIBLE CASE*

DENSITY INDEPENDENT OF PRESSURE
DENSITY DEPENDENT ON TEMPERATURE

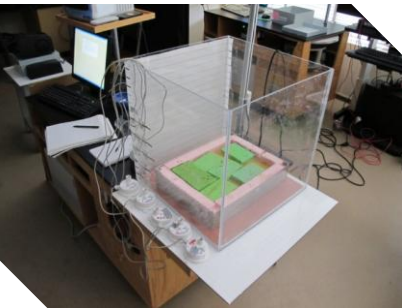


COMPRESSIBLE CASE

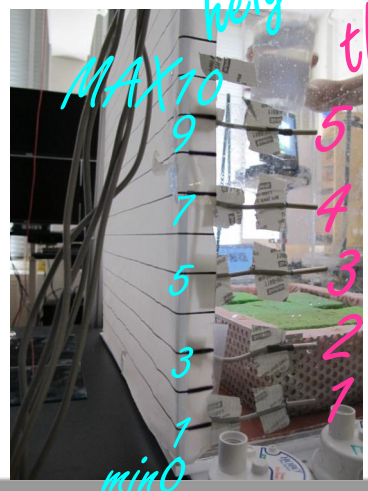


AN INITIALLY STABLY STRATIFIED FLUID CONVECTION SETUP

- OBSERVER RECORDS
- THERMOCOUPLES (4)
- HUMAN -TRANSCRIPT-
- CAMERA [VIDEO]



TANK: TWO



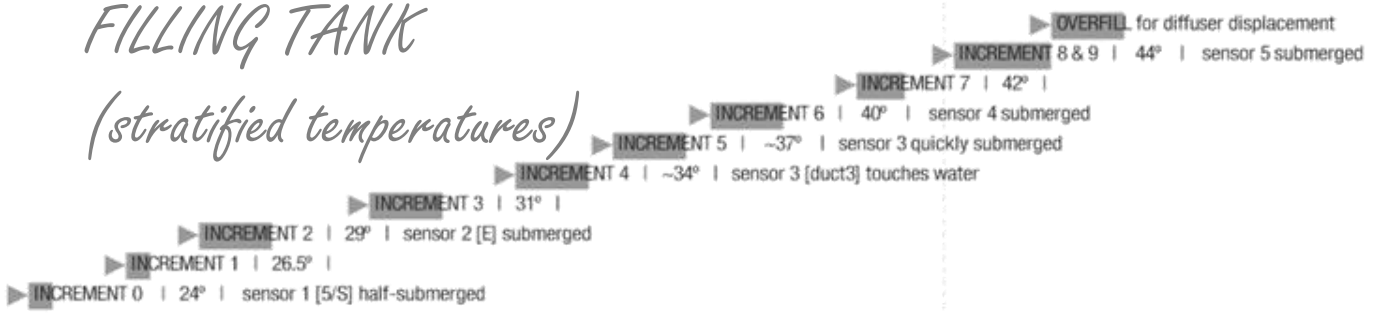
height markers
thermocouples



FILLING TANK

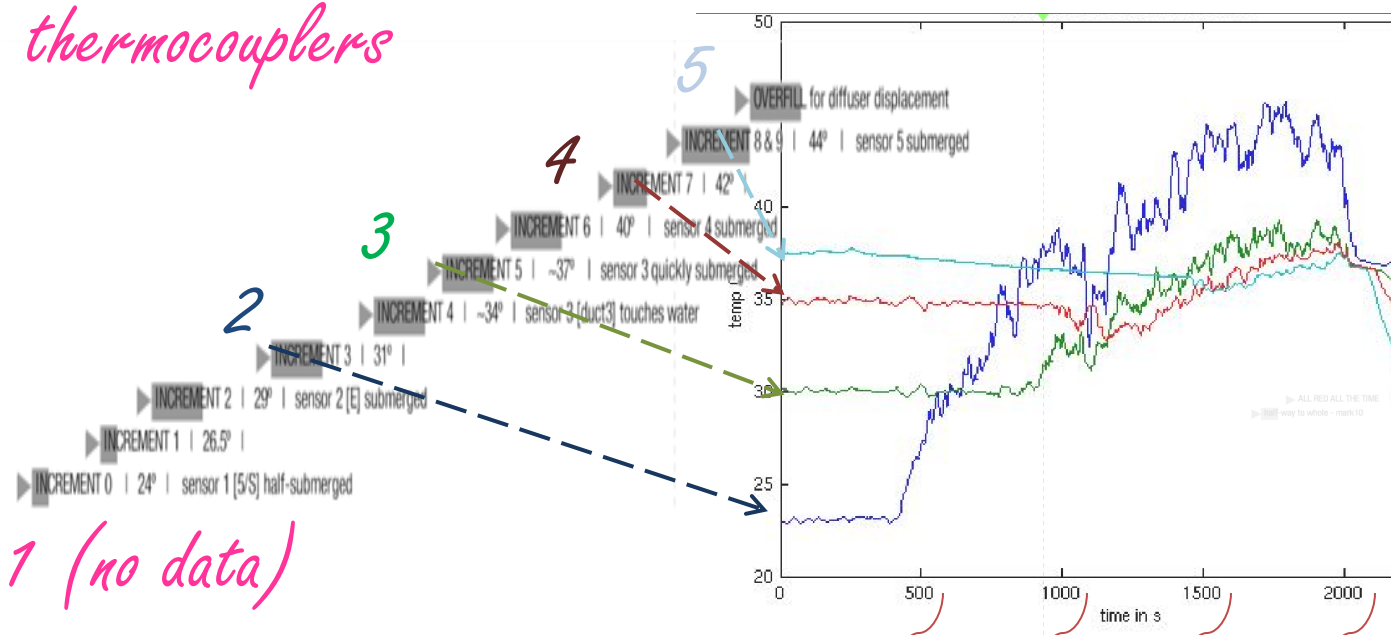
heat on @ 4:10
HEATING

FILLING TANK (stratified temperatures)



FILLING + HEATING TANK

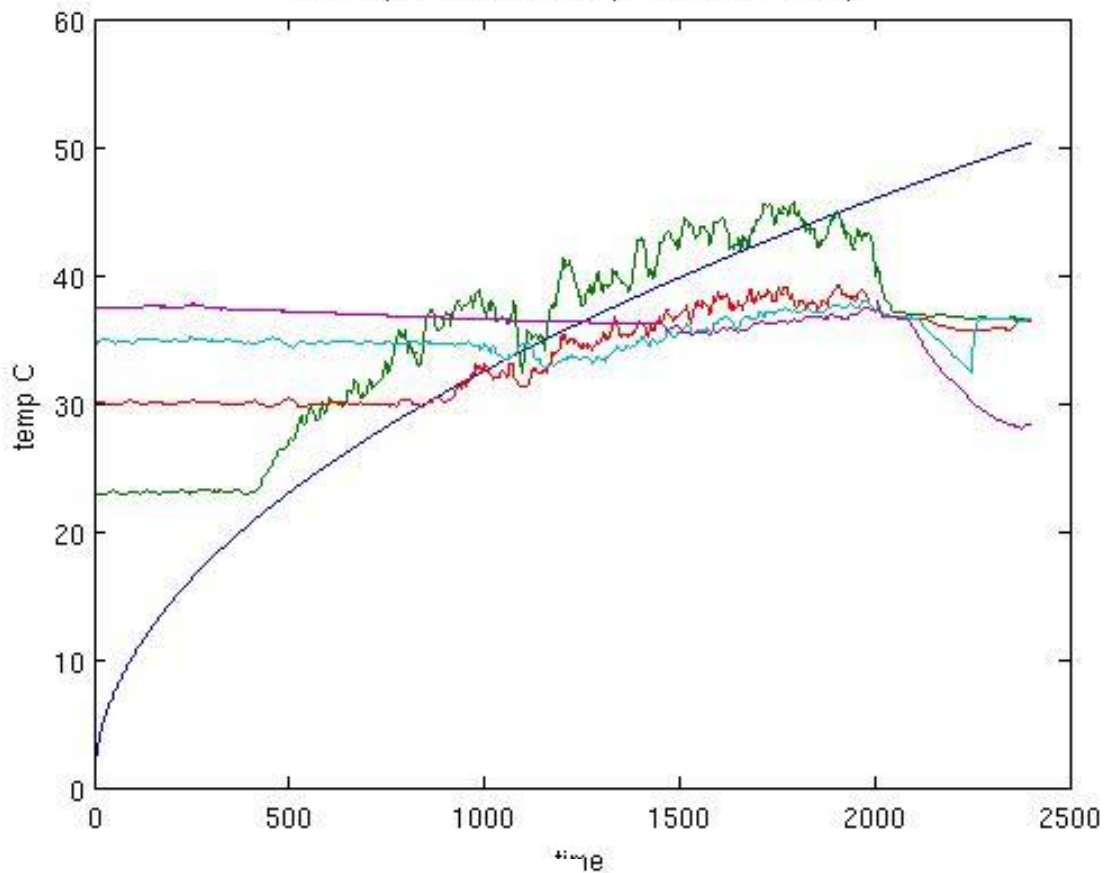
thermocouples



1 (no data)

HEAT SRC heat on @ 4:10 HEATING

Linearly stratified fluid experiment and theory



$$h = \left(\frac{2\mathcal{H}t}{\rho c_p \overline{T_z}} \right)^{\frac{1}{2}}$$

FROM THIS, WE MAY CLAIM $h \propto t^{1/2}$

HEIGHT OF CONVECTIVE LAYER SHOULD BE PROPORTIONAL TO THE SQUARE ROOT OF TIME

WE COULD ATTEMPT PROOF OF THIS IN A VARIETY OF WAYS.

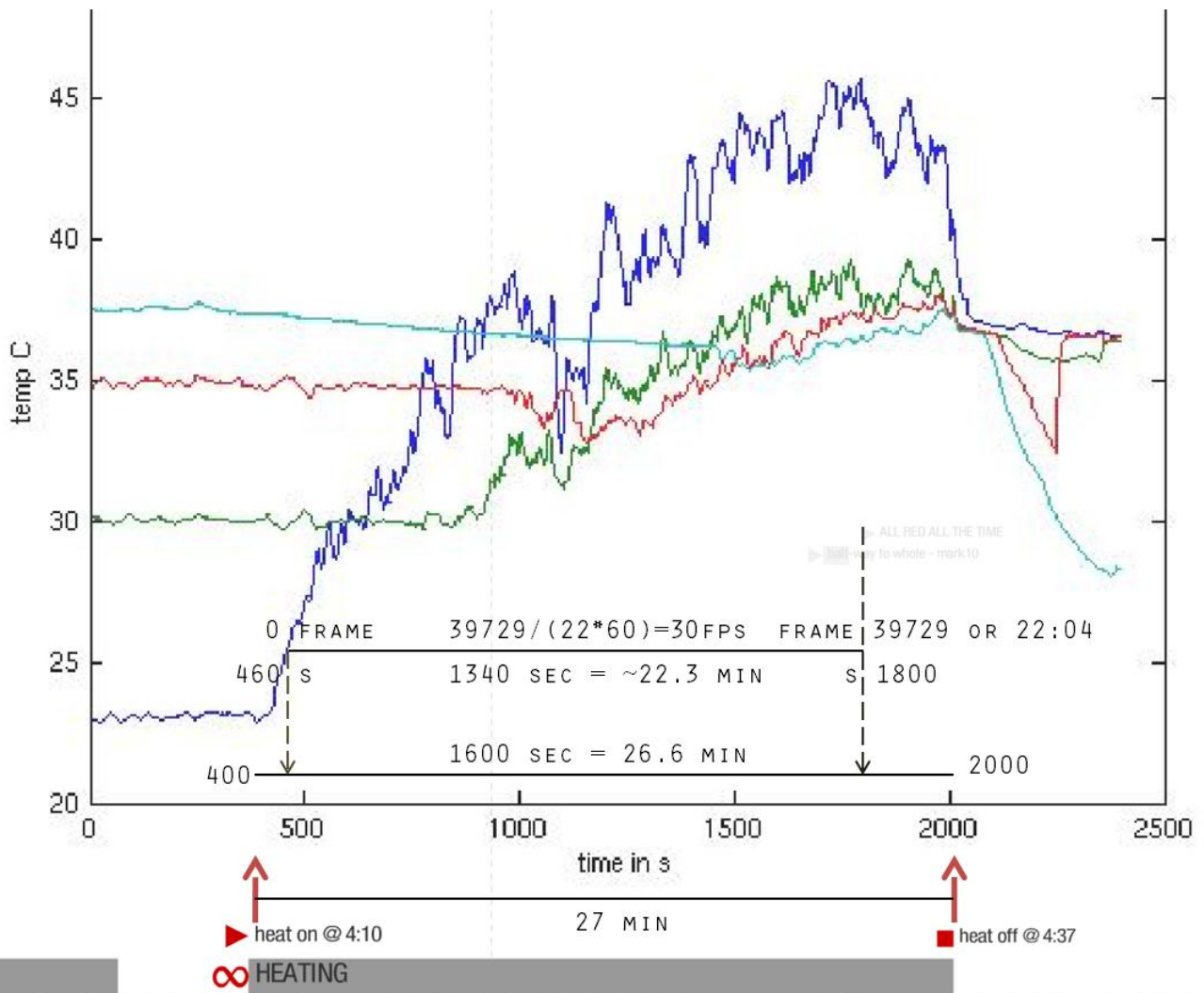
$$h^2 \propto t$$

$$\ln[h] \propto (1/2)\ln[t]$$

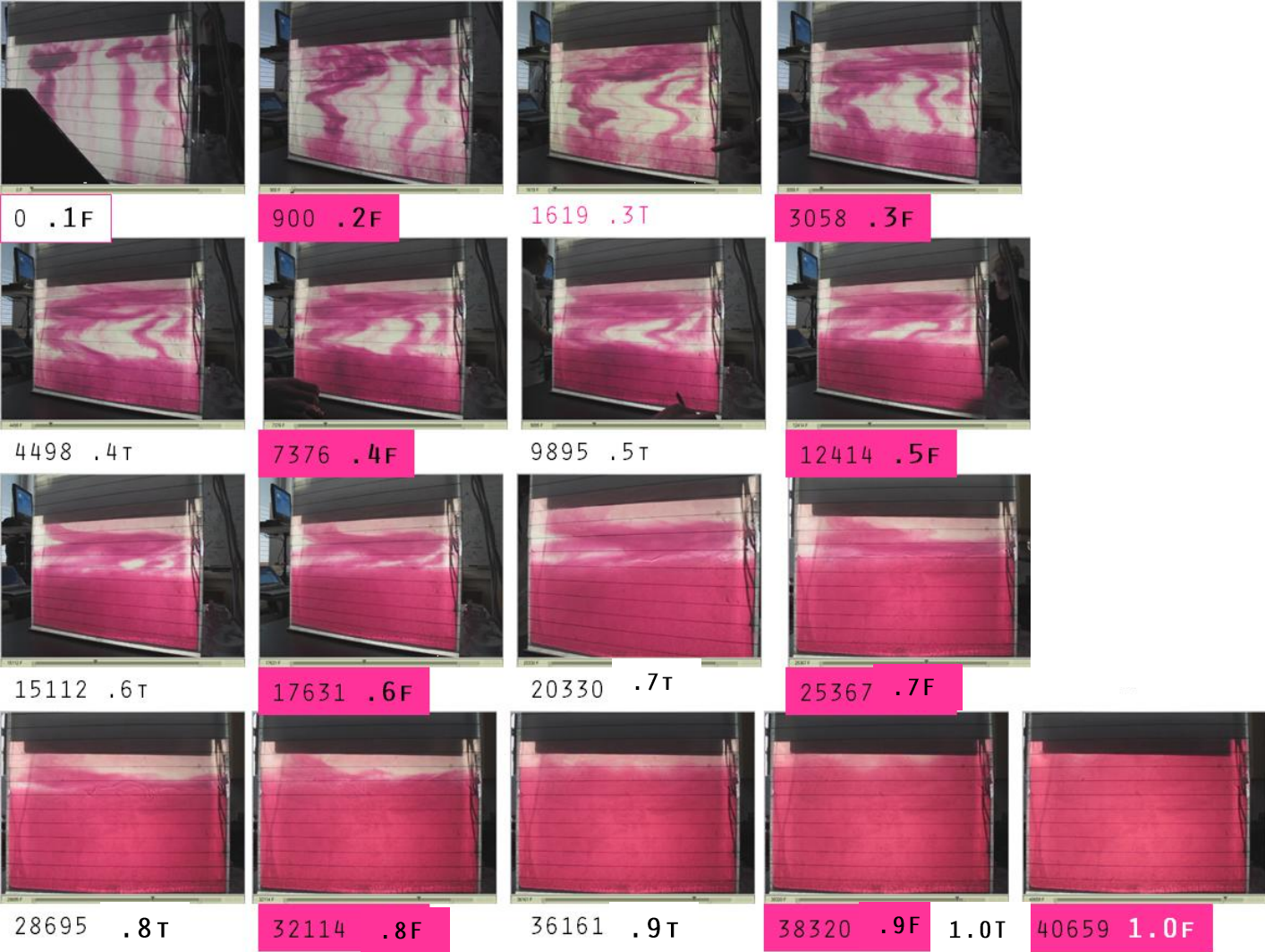
$$\frac{dh}{dt} \propto \frac{1}{2} t^{-1/2}$$

LET'S WORK WITH THE FIRST, ARGUABLY THE SIMPLEST TO CHECK.
 THE LOGARITHM ROUTE WAS OFTEN TAKEN IN CLASS.
 LOGARITHM / POWER RELATIONSHIP WOULD GIVE US A DIRECTION CONSTANT OF PROPORTIONALITY, THAT A LINEARIZATION MIGHT NOT HAVE WITH IT'S Y-INTERCEPT?

LET'S WORK WITH THE FIRST, ARGUABLY THE SIMPLEST TO CHECK.



TIME CALIBRATION OF VIDEO LOGS
WITH HUMAN TRANSCRIPT & THERMOCOUPLE LOGS



SIGNIFICANT VIDEO FRAMES OF CONVECTION IN A TANK
WITH LINEARLY STRATIFIED TEMPERATURE.

“F” OR PINK TAGS TELL WHEN A HEIGHT MARKER HAS BECOME ENTIRELY FILLED (LIKELY OR SOON TO BECOME “NEUTRALIZED”) BY THE CONVECTIVE PROCESS.

FRAME (F#)

HEIGHTMRK (.H)

“T” OR WHITE TAGS TELL WHEN A HEIGHT MARKER BEEN TOUCHED (BY BUOYANTLY RISING & PROMPTING INVERTING PLUMES) BY THE CONVECTIVE PROCESS.

FRAME (F#)

HEIGHTMRK (.H)

LEADING LAG @ FWG

WHEN FIT WITH A REGRESSION, THE DATASET SO FORMULATED WILL GIVE A RELATION IN STRANGE UNIT: %² OF WATER'S HEIGHT / FRAME

THIS CAN BE CONVERTED INTO CM OR M/S, BUT THIS IS UNNECESSARY IN DETERMINING WHETHER THE TWO NUMBERS ARE PROPORTIONALLY RELATED. THIS IS WHERE I REALIZE LOGARITHMS MIGHT HAVE BEEN A SAFER BET FOR PROVING THE PROPTO

LATE START IN VIDEO CAPTURE + IMMEDIACY OF CONVECTION NEXT TO HEAT SOURCE SUGGESTS SETTING A LOWER BOUND ON DATA SET WILL GIVE THE MOST ACCURATE FIT

	≤ 0	10	≤ 0	
450				900
1169	~450 INTERPOLATED, NOT RECORDED	20	900	2158
2879	1619	30	3058	4318
5397	4498	40	7376	5038
5217	9895	50	12414	5217
5218	15112	60	17631	7736
8365	20330	70	25367	6747
7466	28695	80	32114	6206
2159	36161	90	38320	2339
	38320	100	40659	

BETWEEN MARKS 5 AND 6, THE BUOYANT PLUMES AND THE CONVECTION'S NEUTRALIZATION ROSE AT THE SAME RATE

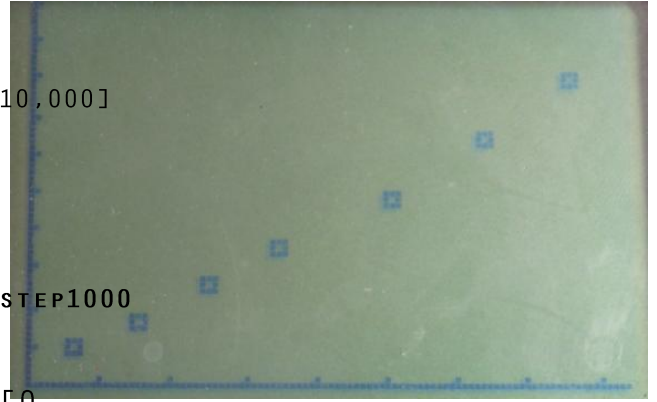
SIMILAR THRESHOLD EFFECTS MAKE REMOVING OUR DATASETS ENDPOINTS AN APPEALING OPTION FOR CONFIRMING THE PROPORTIONALITY OF THE PROCESS' OPERATION

IF THE HEIGHT IS RELATED TO THE SQUARE ROOT OF TIME, IF WE SQUARE OUR HEIGHT, WE SHOULD GET A LINEAR RELATIONSHIP BETWEEN THAT & THE FRAME NUMBER THAT IMPLIES THEY ARE PROPORTIONALLY RELATED TO EACH OTHER.

THERE ARE OBVIOUSLY SOME SUBTLETIES IN THE FLUCTUATING RATES OF THE CONVECTIVE LAYER AND ITS RISING PLUMES THAT WOULD WARRANT DEEPER INVESTIGATION THROUGH CALCULUS METHODS.

DATASET 2
**"TOUCHING/
 LEADING"**

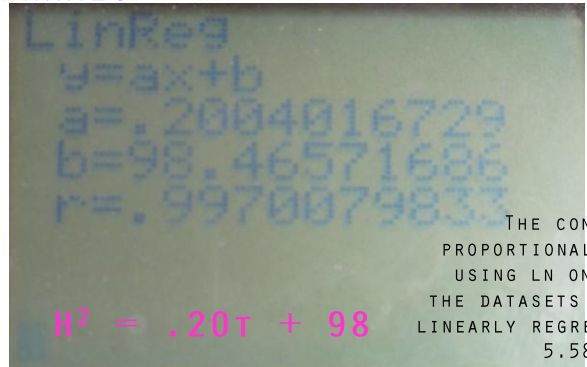
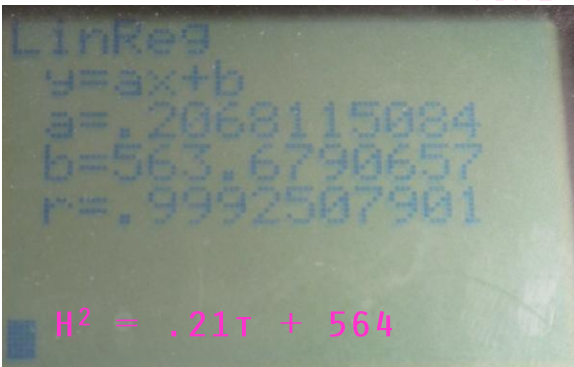
DATASET 1
**"FILLING/
 LAGGING"**



Y: H%² = {900, 1600,
 2500, 3600, 4900, 6400,
 8100}

X: F# = PLOT [DATASET2,1]

[0
 [0 STEP5000 42,000]



THE CONSTANT OF
 PROPORTIONALITY WHEN
 USING LN ON BOTH OF
 THE DATASETS AND THEN
 LINEARLY REGRESSING IS
 $5.58 * [1/2]$
 $= 2.79$
 WITH A +C OF -2. THE
 R VALUE FOR LN IS .992

$$h^2 = .20t + C$$

$$h \propto .45\text{SQRT}(t)$$

R VERY CLOSE TO 1 TELLS THAT THE POINTS ALIGN VERY, VERY CLOSELY ALONG A LINE. THE LEADING BUOYANT PLUME IS A LITTLE "MORE LINEAR" BUT THIS IS HARD TO EXTEND INTO A GENERAL PRINCIPLE BECAUSE OF THE ACCURACY OF OUR INITIAL FRAME SELECTION AND HOW "FILLED" A FILLED LAYER MUST APPEAR. YOU MIGHT SAY THAT THE PLUMES ARE GUIDING OR BUILDING THE ADVANCEMENT OF THE FILLED LAYER; IN ADDITION, IT IS EASIER TO SEE THE "FIRST CONTACT" VERSUS "GENERALLY FILLED" BEING MUCH MORE SUBJECTIVE QUALIFIER.

FRAMES

0

VIDEO

15000

+500s

20000

+666s



400

580

760

940

1120

SECONDS

TEMPERATURE PROFILES

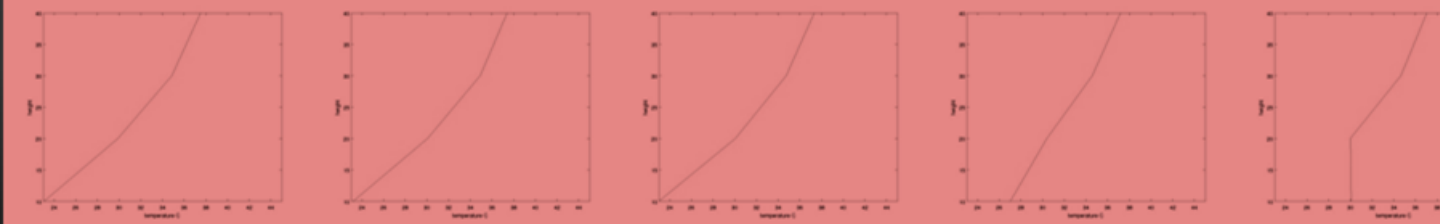
400

600

800

1000

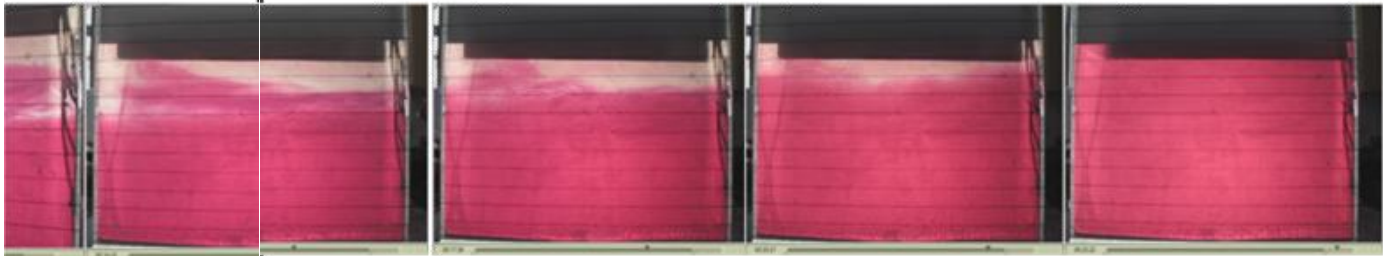
1200



INITIALLY WE SEE THAT THE TEMPERATURE PROFILE OF THE TANK IS STABLE—THIS IS A RESULT OF DELIBERATE CARE PUTTING LAYERS OF INCREASINGLY WARM WATER THROUGH A DIFFUSER TO PREVENT THEM FROM MIXING DUE TO DISTURBANCE. THIS IS THE LINEAR STRATIFICATION OF THE TANK, IT IS A CONFIRMED TO BE A STABLE CONFORMATION BECAUSE $dT/dz > 0$

BY 1200 SECONDS, WE CAN SEE THE CONVECTION HAS PROCEEDED, OVERTAKING AT LEAST VISUALLY THE 6 LOWERMOST VERTICAL MARKERS TANKSIDE [.6F OR 60% USING THE INVENTED NOTATION] IN THE PROFILE, THE NEUTRALITY IN THE CONVECTIVE LAYER CAN BE OBSERVED WHERE $dT/dz = 0$. THIS NEUTRALITY ENDS ABOUT ONE THIRD OF THE OVERALL PROFILE, BEFORE IT BECOMES STABLE WHERE $dT/dz > 0$.

THIS IS INTERESTING, AS IT SUGGESTS THE NEUTRALIZING EFFECT MAY, AT TIMES, ONLY CUE US INTO HALF OF THE PHENOMENA'S TOTAL ACTIVE SPAN.



1300

1300

1480

1660

1840

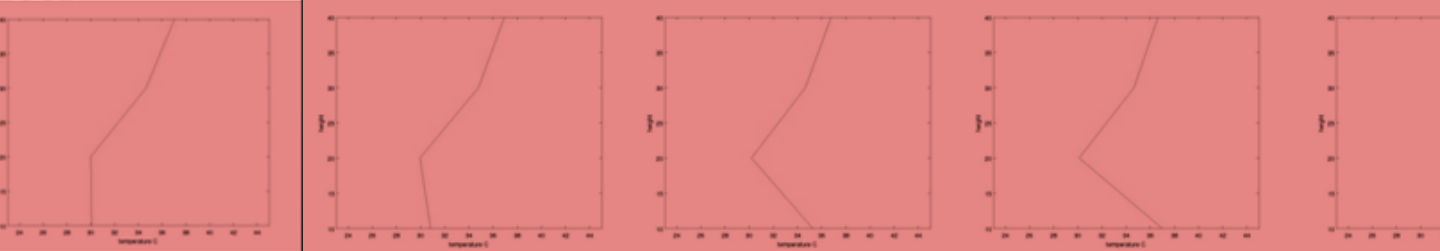
1200

1400

1600

1800

2000



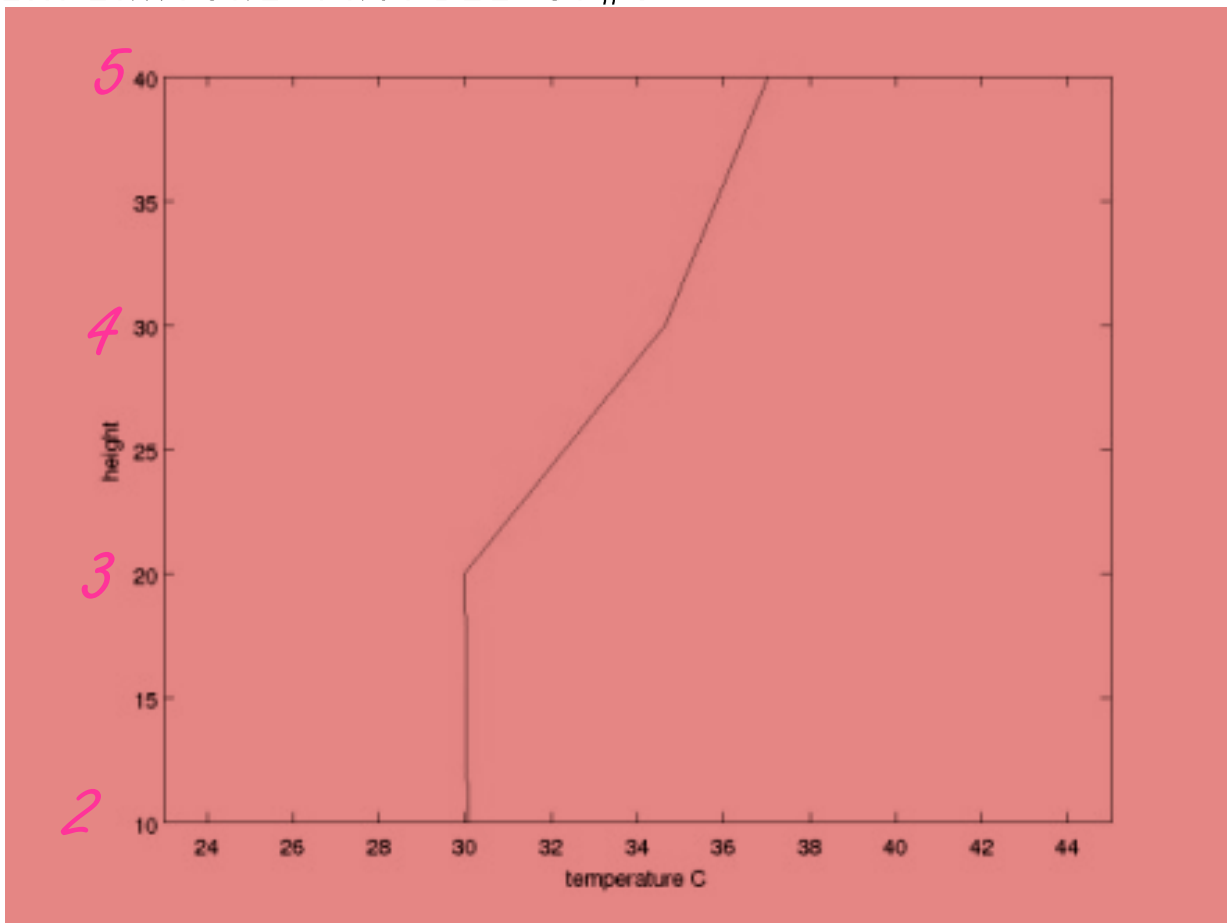


VIDEO @F#: 1120

1300

CLOSER ANALYSIS OF THE GRAPH SHOWS THAT OUR PRIOR ASSUMPTION WAS INCORRECT. THE GRAPH STARTS AT 10 CM, SO THE PLOT WINDOW IS CONCEALING HALF OF THE CONVECTIVE LAYERS NEUTRALIZATION. THIS IS MUCH MORE IN LINE WITH WHAT WE ARE OBSERVING IN VIDEO TO THERMOCOUPLE RELATION.

TEMPERATURE PROFILE @F#: 1200



AVG HT 4.5 UNIT



14s/4.5BARS
= 3.11 S/BAR

13.9 OR ~14s

416F AVG

325 425 400 400 430 512 440 413 395 380 450 450 390 5410/13

BETWEEN 15000 - 20000, TOOK 13 MEASUREMENTS OF FRAMES FOR A CONVECTION PLUME TO RISE

15000
+500s

20000
+666s



760

940

1120

1300

LAW OF VERTICAL HEAT TRANSPORT.

$$H = PC_pWT$$

RESEARCH STUB.

$$H = 1600W$$

$$W = .32 \text{ BARS / SECOND}$$

$$\text{HEIGHT OF A BAR} = \sim 5\text{CM}$$

T OBTAINABLE FROM GRAPH ON PRIOR PAGE.

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ENVIRONMENTS

ATMOS:ONE 3

COMPRESSIBLE CASE



THEORY

MODELS

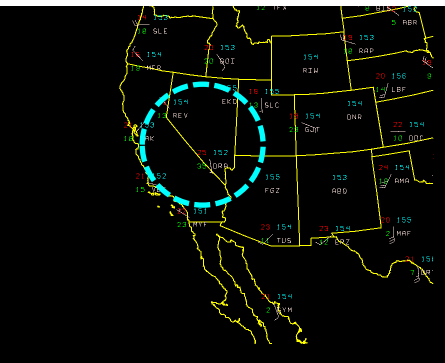
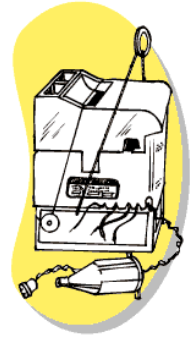
OBSERVATIONS

CONVECTION

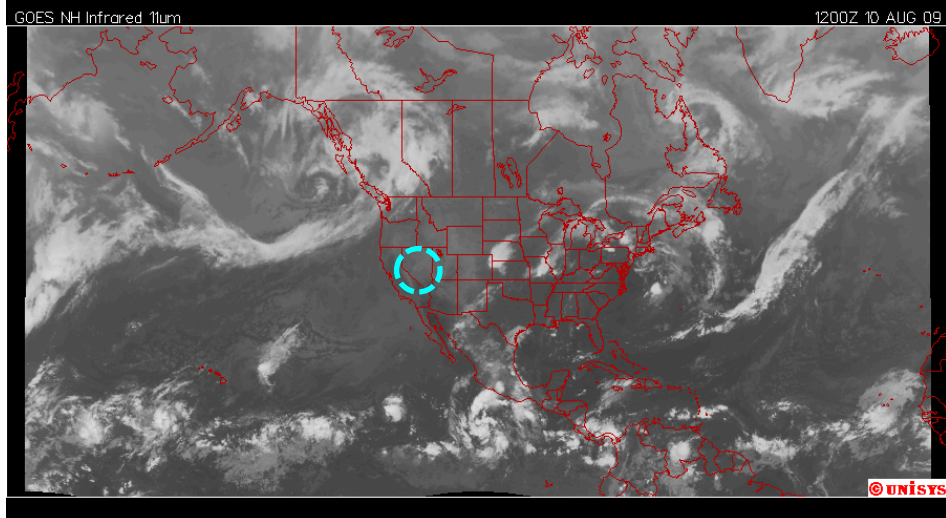
OBSERVER RECORDS

SATELLITES

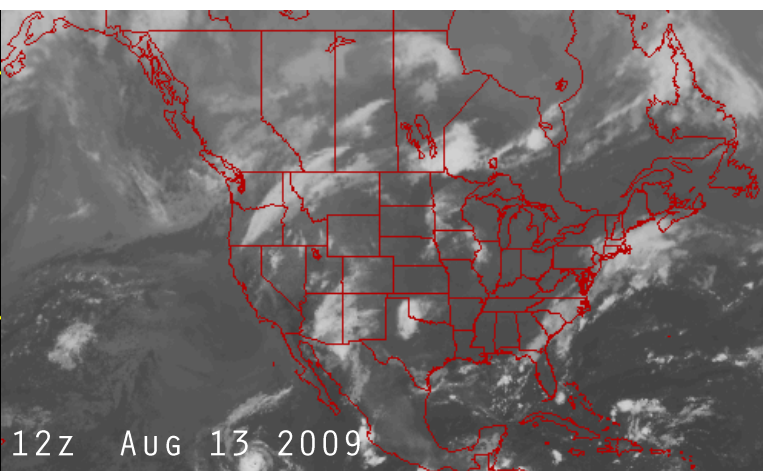
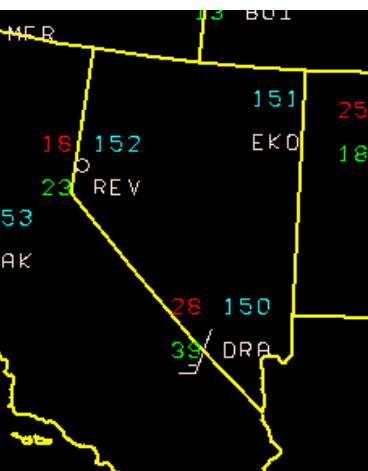
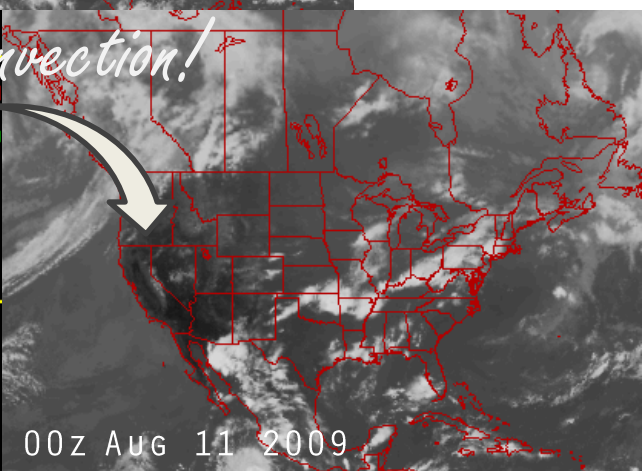
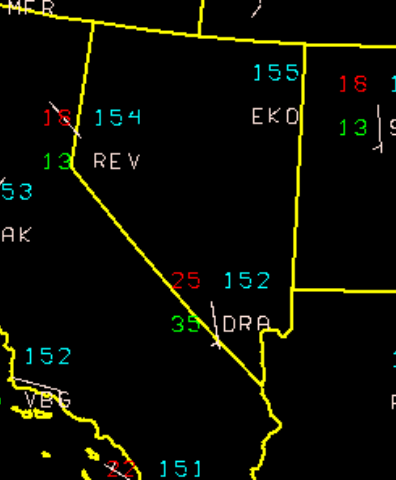
RADIOSONDES



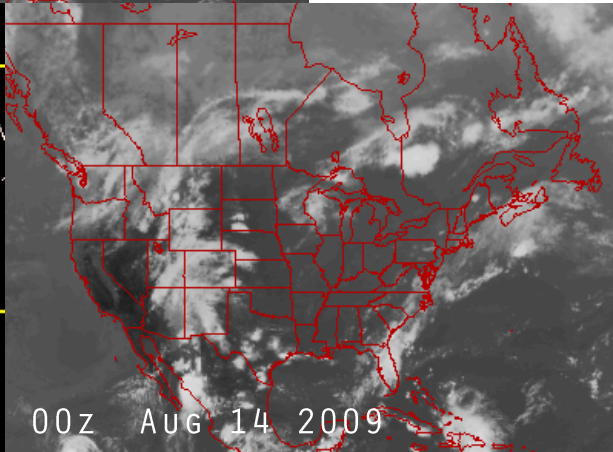
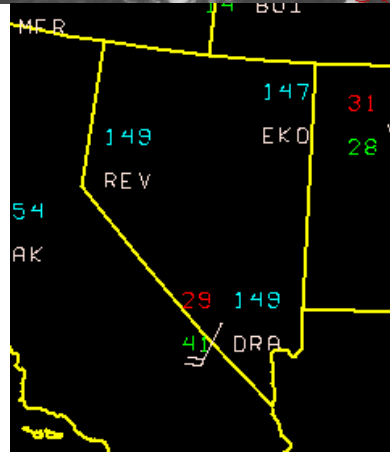
WE SEEK DRY AIR CONVECTION, AS MOISTURE IN THE AIR ADDS AN ADDITIONAL LEVEL OF COMPLEXITY



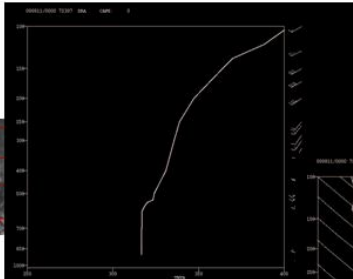
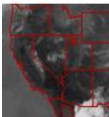
WATER VAPOR IMAGERY CONFIRMS VERY LITTLE MOISTURE IN THE SOUTHWEST ON AUGUST 10, 2009.



14 LOOKS DRY, BUT ALSO CLOSE TO A WEATHER SYSTEM. QUICK STUDY OF WHICH OFFERS THE BETTER EXAMPLE OF CONVECTIVE NEUTRALIZING



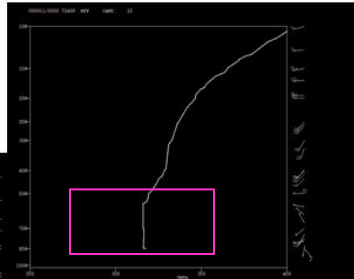
11



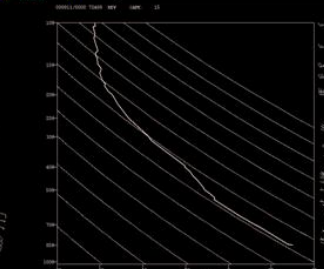
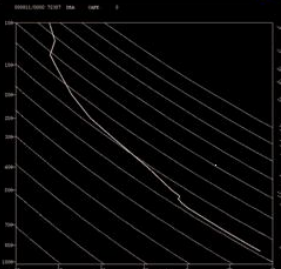
REV



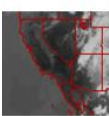
DRA



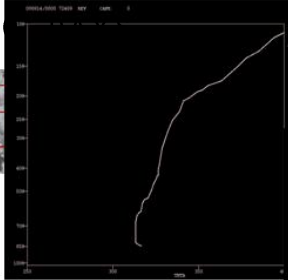
TWO MEASURES



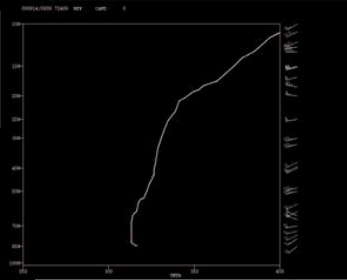
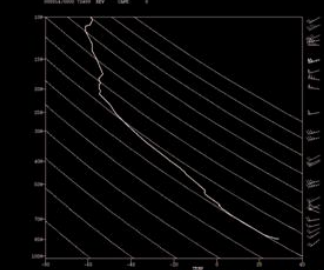
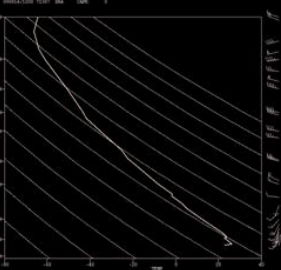
TW



14



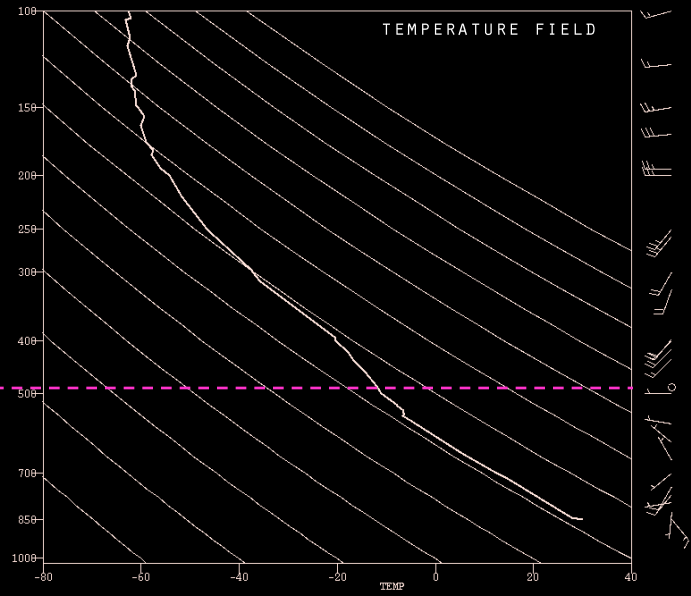
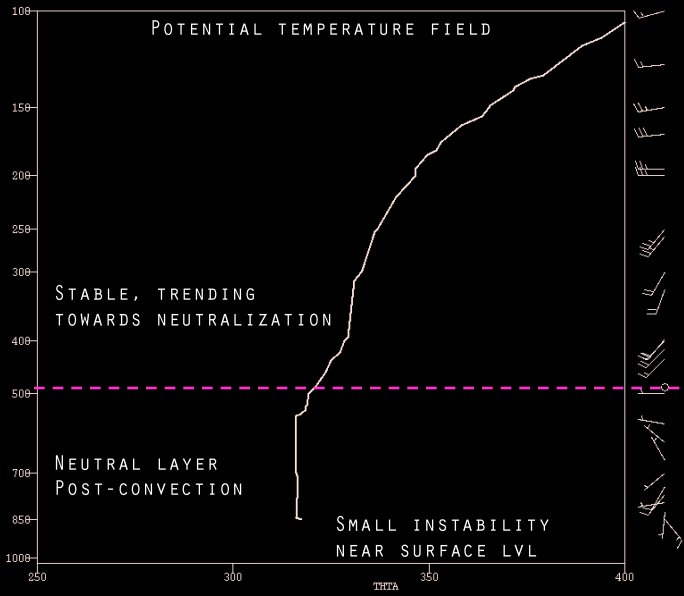
TWO CITIES



AUG 11 2009 00z

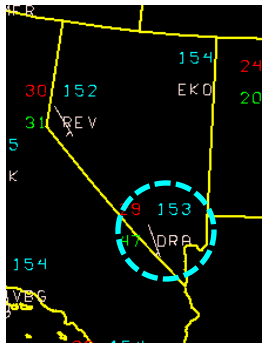
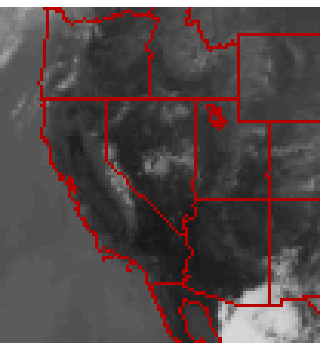
090811/0000 72489 REV CAPE: 15

090811/0000 72489 REV CAPE: 15



$$\theta = T \left(\frac{p_0}{p} \right)^\kappa$$

UNSTABLE } if $\left(\frac{d\theta}{dz} \right)_E < 0$
NEUTRAL } $\left(\frac{d\theta}{dz} \right)_E = 0$
STABLE } $\left(\frac{d\theta}{dz} \right)_E > 0$



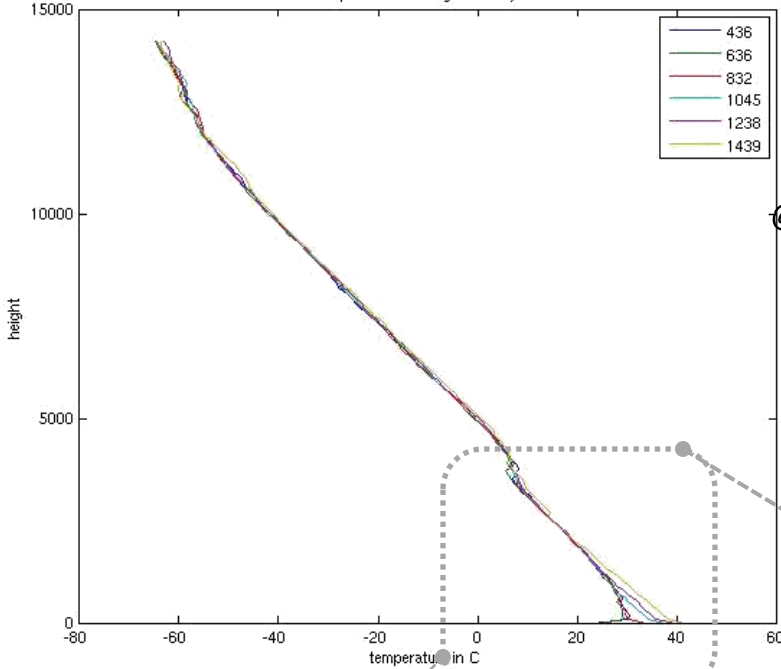
DRA

ATMOS:TWO 4

RADIOSONDES (6)

1136Z
 1336Z
 1532Z
 1745Z
 1938Z
 2139Z

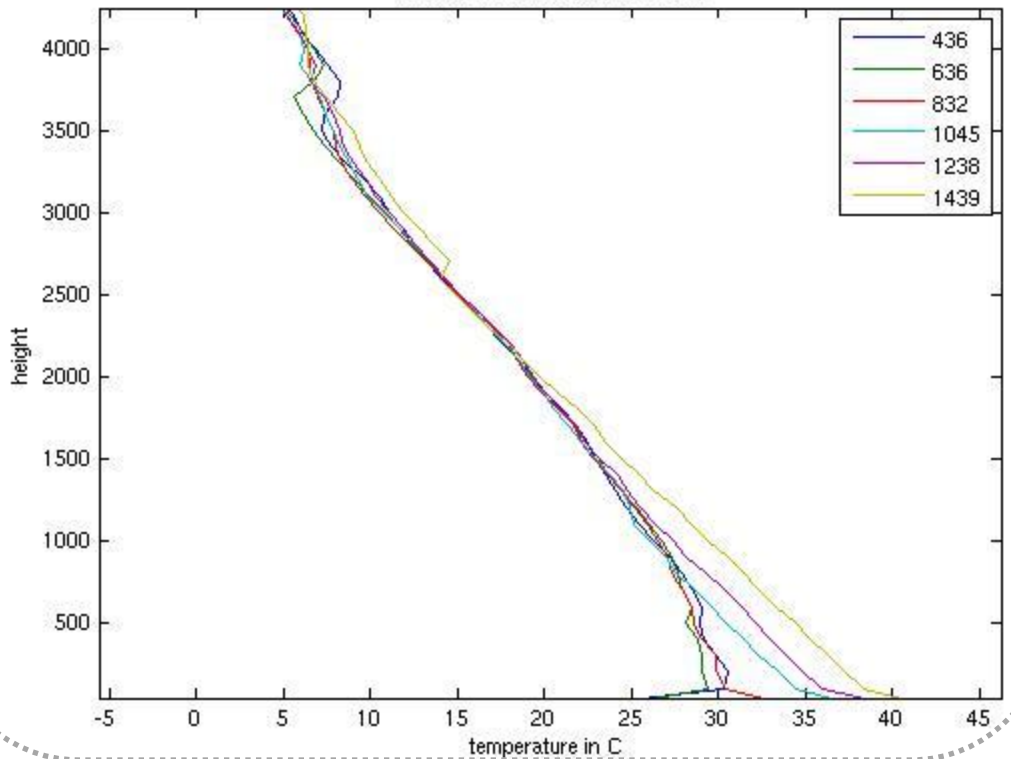
Temperature vs. height: Yuma, AZ



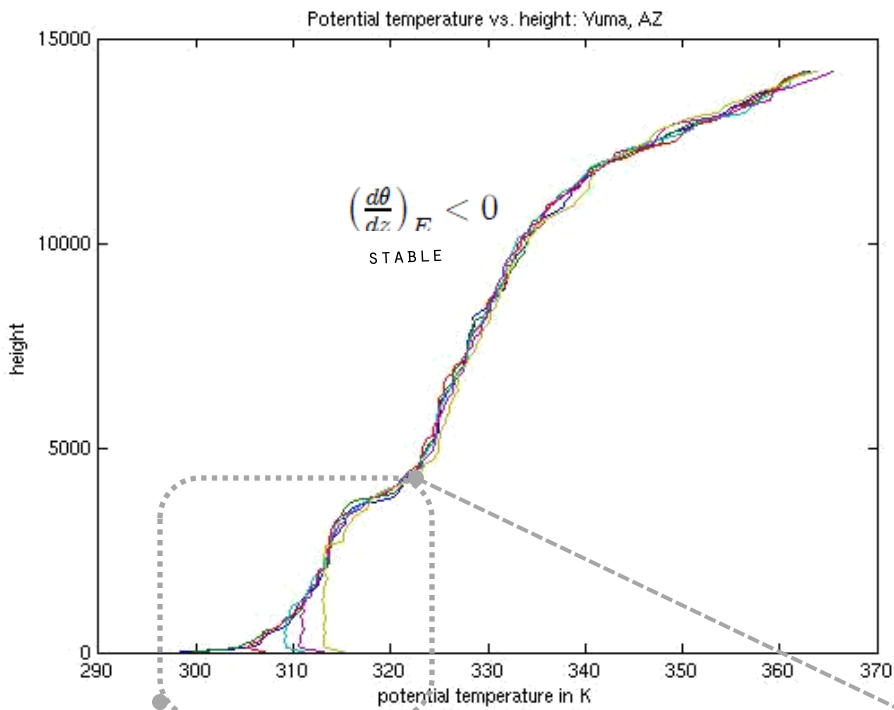
@ YUMA, ARIZONA
 JUNE 18, 2007 GMT -7

AS WE MIGHT EXPECT, THE TEMPERATURE AT THE SURFACE INCREASES THROUGHOUT THE DAY FROM MIN~25 TO MAX~40 DEGREES C. BUT THIS TELLS US VERY LITTLE ABOUT THE PROGRESSION OF THE CONVECTIVE BOUNDARY LAYER THROUGHOUT THE DAY.

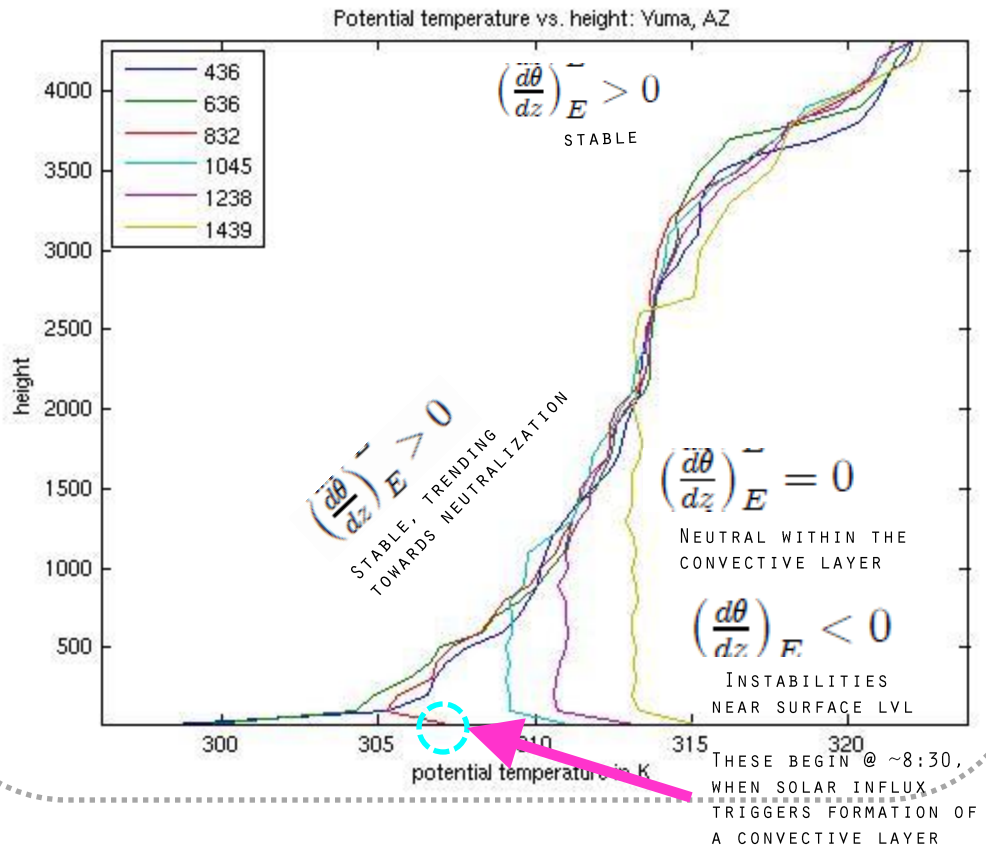
Temperature vs. height: Yuma, AZ



VERTICAL PROFILES OF TEMPERATURE FOR SIX RADIOSONDE RELEASES



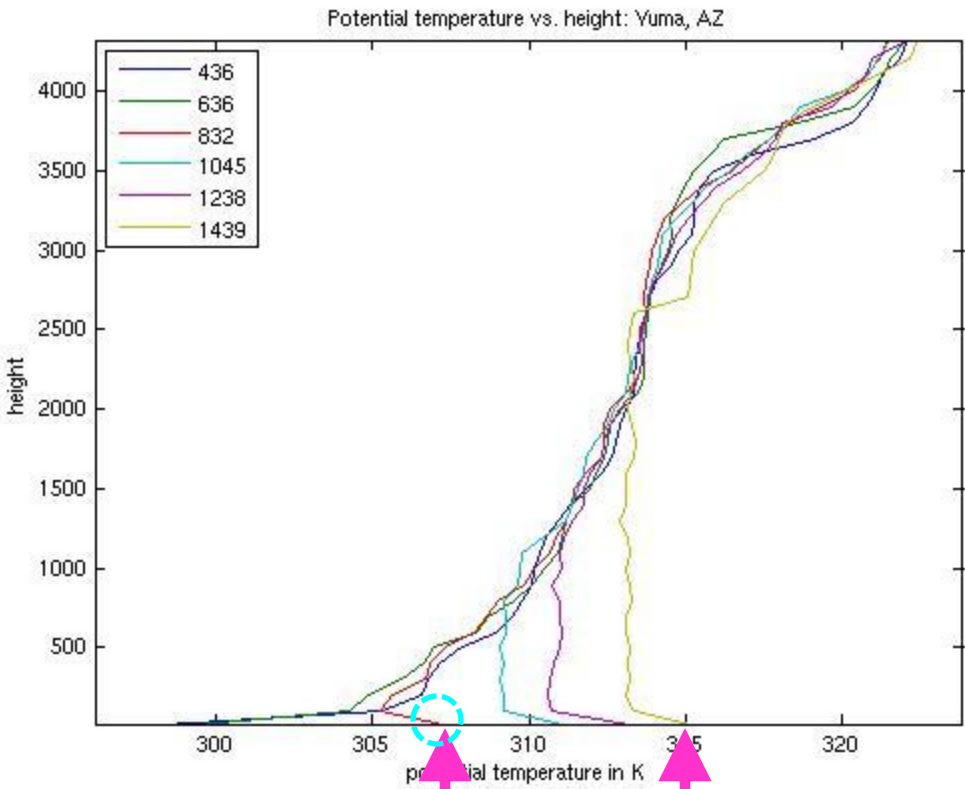
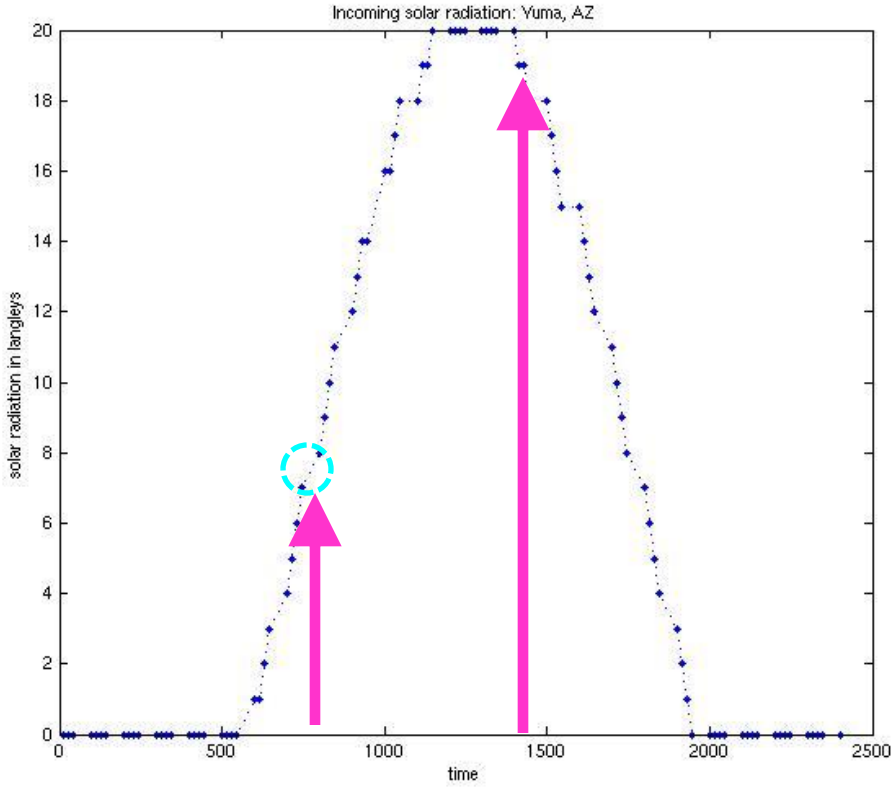
FOR THAT WE TURN TO POTENTIAL TEMPERATURE. AS WE OUTLINED IN THE NEVADA CASE JUST PRIOR, YOU CAN IDENTIFY UNSTABLE PARTS OF THE CONVECTION CLOSE TO THE SURFACE [ANALOGOUS WITH RAPID PLUMES AT HEATING PAD] FADING INTO A NEUTRALIZED ZONE THAT GROWS OVER THE COURSE OF THE DAY, AGAIN IN LINE WITH OUR EXPERIENCES VIEWING THE TANK'S OUTWARDLY VISIBLE PROGRESSION AND INWARDLY SENSED TEMPERATURE PROFILES.



VERTICAL PROFILES OF POTENTIAL TEMPERATURE FOR SIX RADIOSONDE RELEASES

$$H\Delta t = \frac{c_p}{g} \sum_{i=1}^N \Delta T_i \delta p_i$$

THE SURFACE INVERSIONS THAT INITIATE THE CONVECTIVE CELL MAY BE RELATED TO A THRESHOLD OF INCOMING SOLAR RADIATION (SAY, 8 HADLEYS), BUT IT'S LIKELY ALSO IMPACTED BY THE ACCUMULATED INTEGRAL OF SOLAR RADIATION THAT DAY - SAY, WHAT MINIMUM ENERGY IS NECESSARY IN ORDER TO GIVE PARCELS OF AIR WITH ENOUGH BUOYANCY TO RISE INTO NEXT LAYER, CREATING THE OVERTURNING, NEUTRALIZING MOTION.



BY THE TIME IT IS PAST THE PEAK OF SOLAR RADIATION NEUTRALIZATION HAS PROGRESSED UPWARDS OF 2500 FT.

